

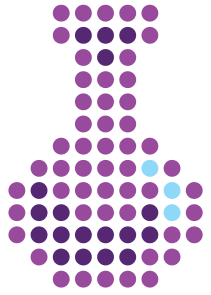
sck cen

Belgian Nuclear Research Centre



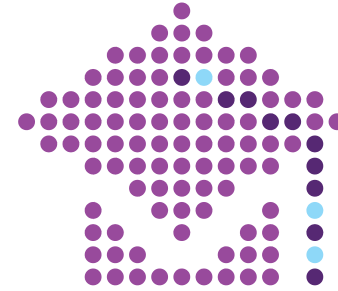
# Reactor produced medical radionuclides

Michiel Van de Voorde – PRISMAP School on Radionuclide Production – May 2024



## Outline

- Introduction
- **Basic concepts**
- **Production** strategies
- Radiochemical **processing**



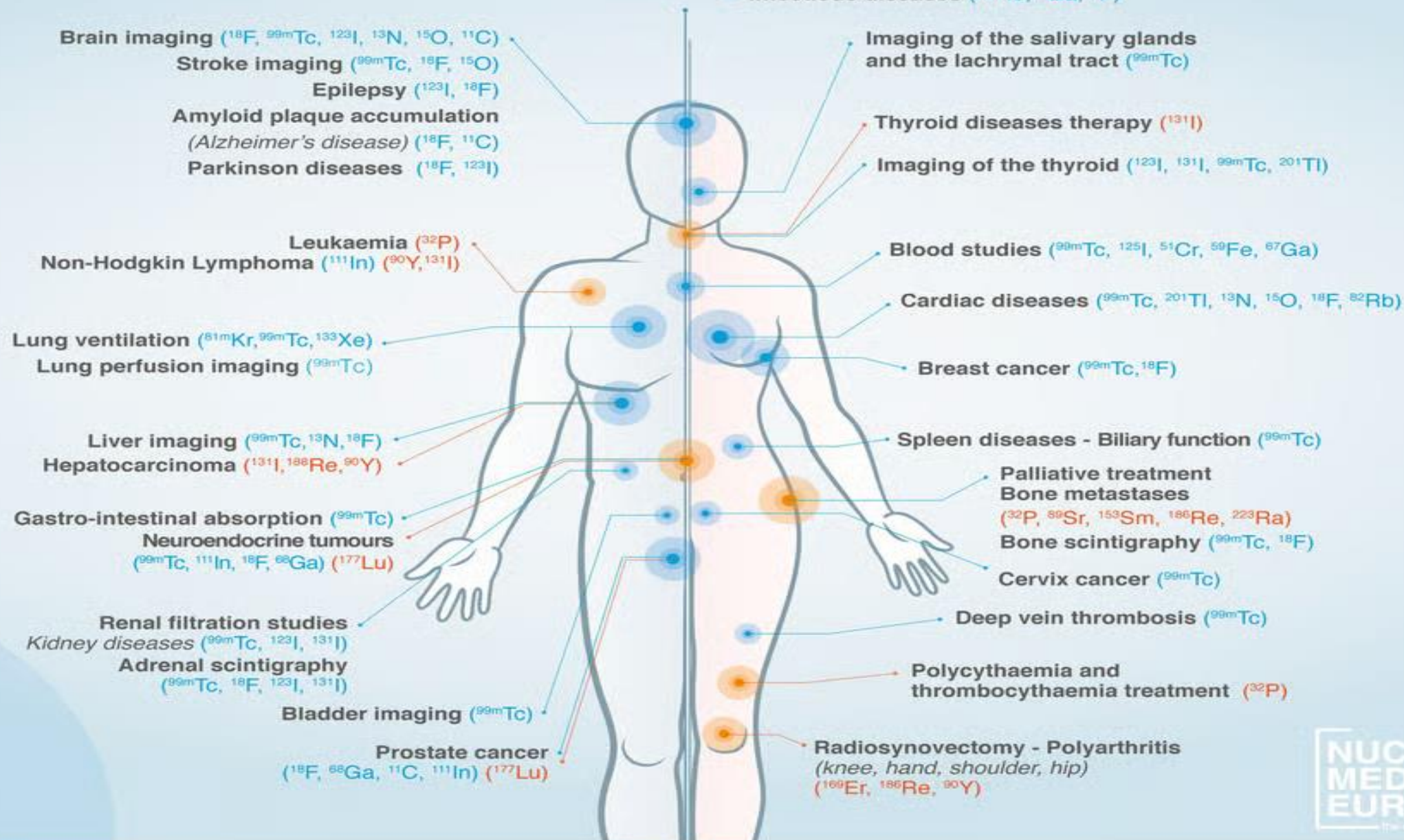
## Learning outcomes

- Know the **difference** between reactor and accelerator produced radionuclides
- **Basic understanding** of how radionuclides are produced in a nuclear reactor
- Estimating a **production yield** and evaluating a **production strategy**

# DIAGNOSIS & THERAPY

## Whole body

- Primary tumors and metastases ( $^{18}\text{F}$ ,  $^{11}\text{C}$ )
- Oncology therapy ( $^{131}\text{I}$ ,  $^{177}\text{Lu}$ ,  $^{166}\text{Ho}$ ,  $^{90}\text{Y}$ )
- Infectious diseases ( $^{99\text{m}}\text{Tc}$ ,  $^{67}\text{Ga}$ ,  $^{18}\text{F}$ )

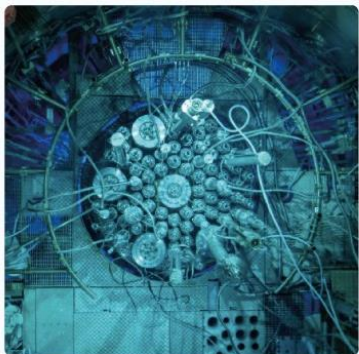


## Cyclotron



or

## Reactor



## Nuclear reaction

or

## Radioisotope production

## Shipment

from reactor  
to production facility

## Radiochemical grade product

from reactor  
to production facility



or

## «Active Pharmaceutical Ingredient» (API)

- Purification
- Quality Control
- Dispensing

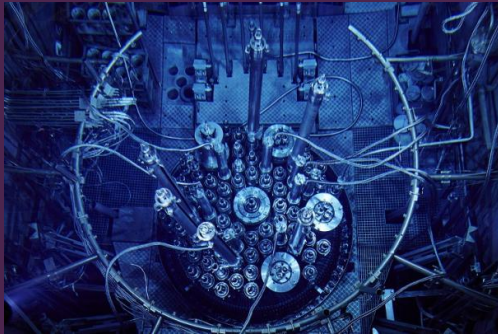


## Radiopharmaceutical product

- Labeling (if required)
- Dispensing
- Sterilization
- Quality Control
- Packaging
- Shipping



# Production methods



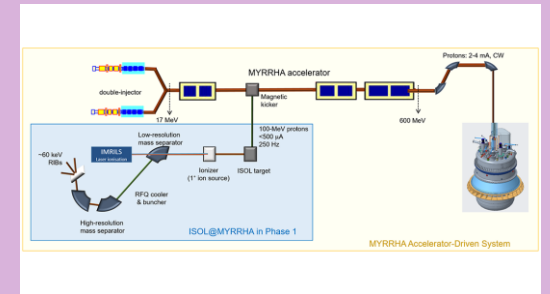
Reactor produced



Cyclotron produced



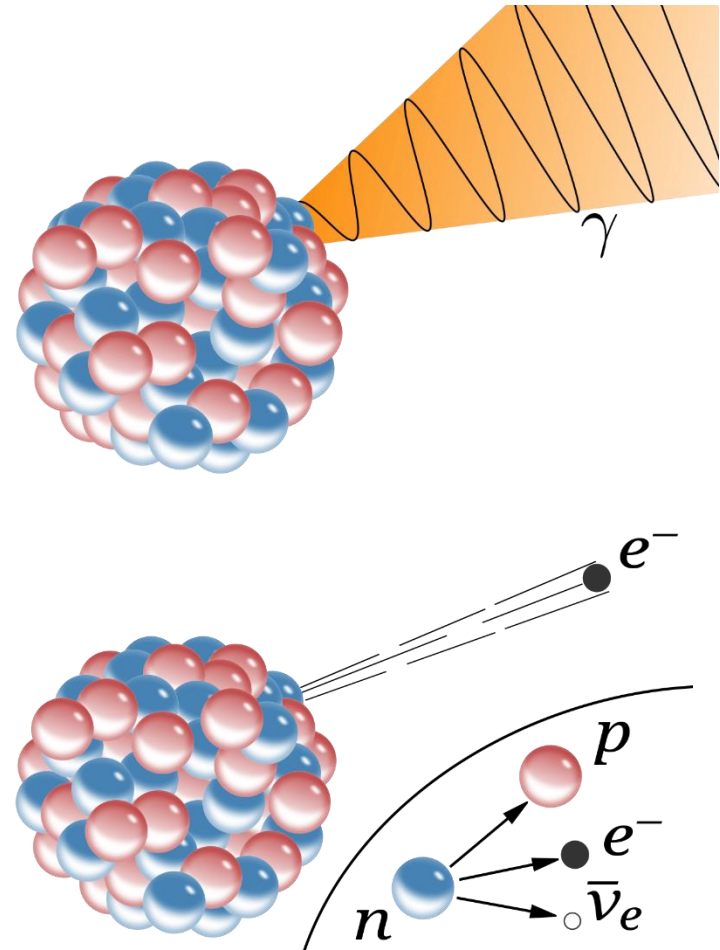
Gamma produced

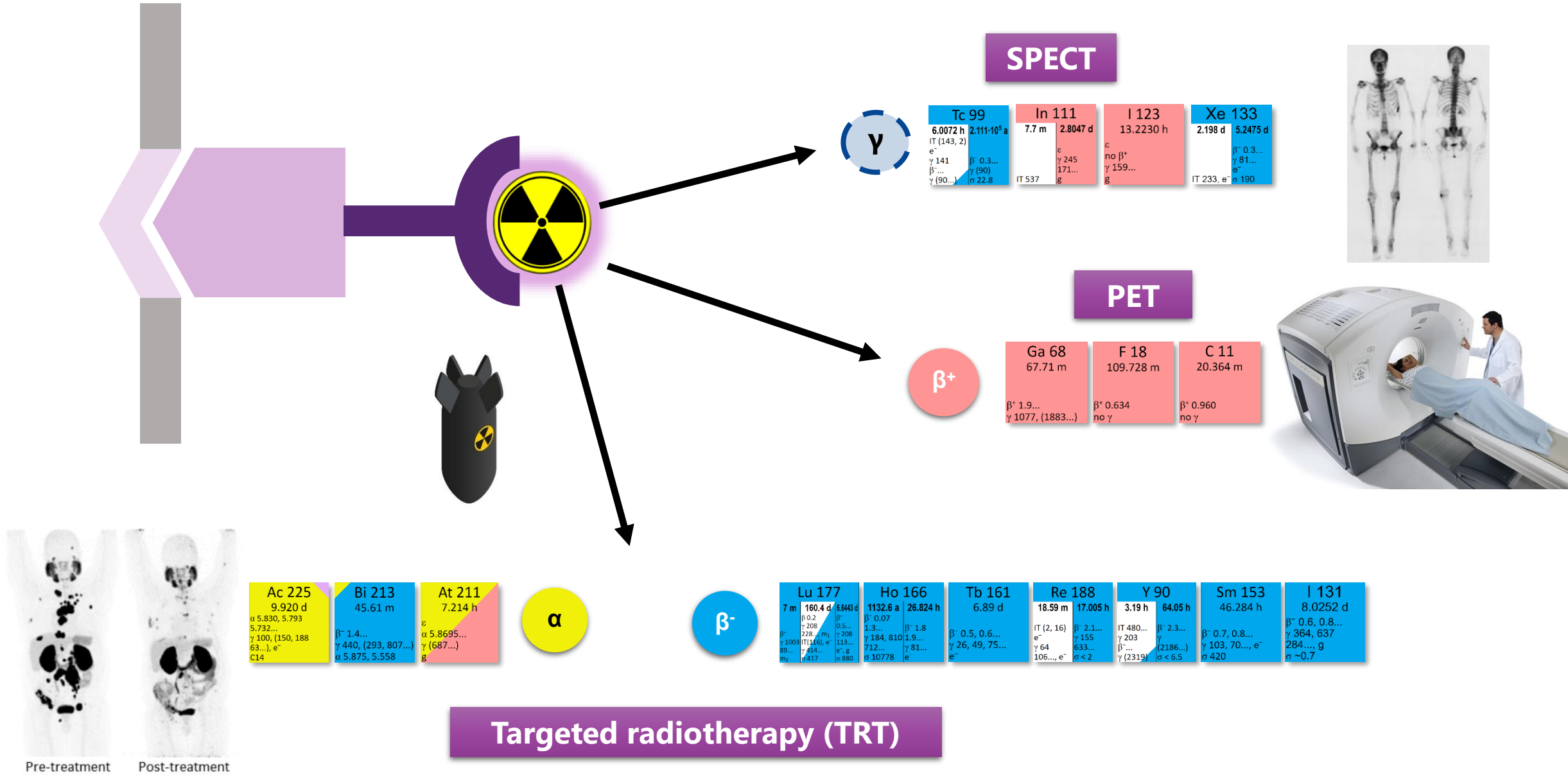


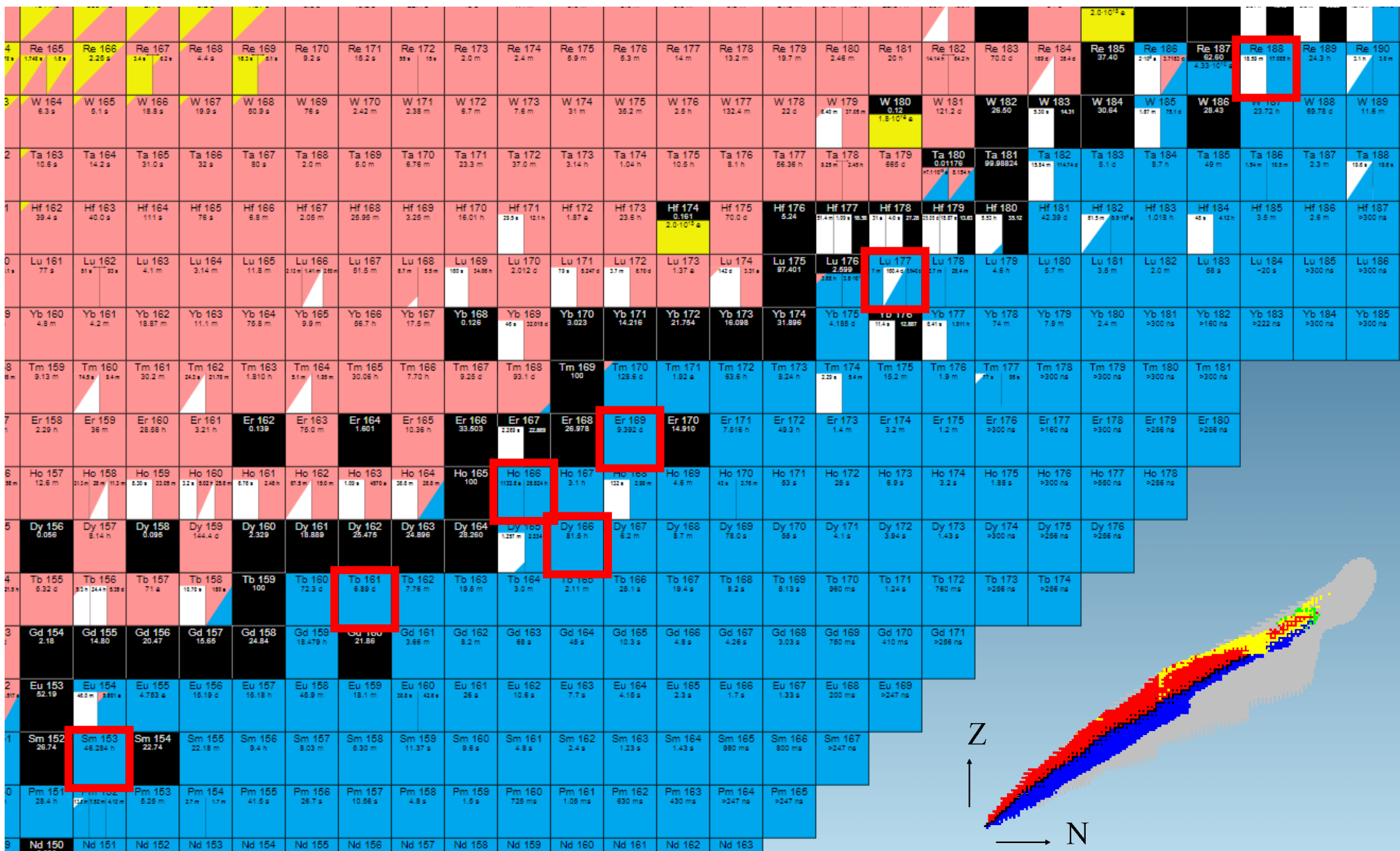
ISOL produced

# General classification

- Radionuclides for SPECT
  - Reactor and cyclotron produced
- Radionuclides for PET
  - Cyclotron produced
- Radionuclides for therapy
  - Reactor produced
  - Naturally occurring
  - Accelerator produced









# Nuclear transmutation

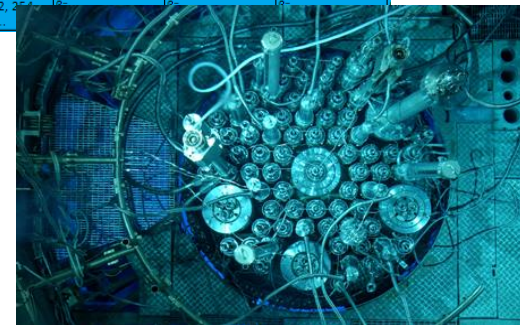
Ho 150 23.5 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Ho 151 72 s 47.2 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Ho 152 35.2 s 50.0 s β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 153 2.01 m 9.3 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 154 11.76 m 3.1 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 155 48 m Ho 156 7.6 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 157 12.6 m Ho 158 21.3 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 159 33.05 m Ho 160 3.2 s β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 161 2.48 h Ho 162 67.5 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 163 4570 a Ho 164 36.6 m β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 165 100 Ho 166 1132.6 a β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...	Ho 167 3.1 h Ho 168 1132.6 a β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551... β <sup>+</sup> 3.2... γ 614 394, 551...																
Dy 149 0.490 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 150 4.20 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 151 7.17 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 152 17 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 153 6.4 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 154 3.0-10 <sup>6</sup> a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 155 9.9 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 156 0.056 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 157 8.14 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 158 0.095 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 159 144.4 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 160 2.329 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 161 18.889 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 162 25.475 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 163 24.896 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 164 28.260 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 165 1.257 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 166 2.334 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Dy 167 81.5 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...									
Tb 148 2.20 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 149 60 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 150 4.2 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 151 4.1 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 152 5.8 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 153 3.48 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 154 25 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 155 17.609 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 156 4.2 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 157 17.5 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 158 2.34 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 159 22.7 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 160 9.994 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 161 21.5 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 162 5.32 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 163 53 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 164 24.4 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 165 5.35 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 166 71 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 167 10.70 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 168 180 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 169 100 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 170 72.3 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 171 6.89 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 172 7.76 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 173 19.5 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 174 3.0 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Tb 175 2.11 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...
Gd 147 38.1 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 148 71.1 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 149 9.28 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 150 1.79-10 <sup>6</sup> a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 151 120 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 152 0.20 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 153 240.4 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 154 2.18 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 155 14.80 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 156 20.47 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 157 15.65 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 158 24.84 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 159 18.479 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 160 21.86 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 161 3.66 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 162 8.2 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 163 68 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Gd 164 45 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...										
Eu 146 4.61 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 147 24.1 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 148 54.5 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 149 93.1 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 150 12.8 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 151 36.9 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 152 96 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 153 9.312 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 154 13.517 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 155 52.19 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 156 46.0 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 157 8.601 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 158 4.753 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 159 15.19 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 160 15.18 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 161 45.9 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 162 18.1 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 163 30.8 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 164 42.6 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 165 10.6 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 166 26 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Eu 167 10.6 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...						
Sm 145 340 d β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 146 6.8-10 <sup>7</sup> a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 147 15.00 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 148 11.25 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 149 13.82 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 150 7.37 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 151 94.7 a β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 152 26.74 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 153 46.284 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 154 22.74 β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 155 22.18 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 156 9.4 h β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 157 8.03 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 158 5.30 m β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 159 11.37 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 160 9.6 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 161 4.8 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...	Sm 162 2.4 s β <sup>+</sup> 3.9... γ 803, 653 394, 551... β <sup>+</sup> 3.9... γ 803, 653 394, 551...										

- Stable
- $\beta^-$  decay
- $\alpha$  decay
- $\beta^+$  decay



Neutron-deficient

Acquired by particle  
accelerators



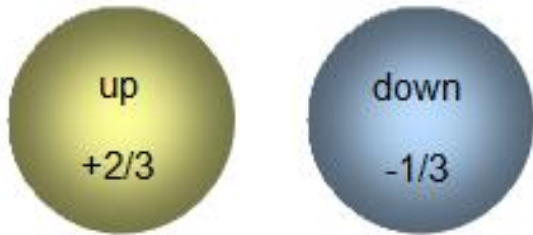
Proton-deficient

Acquired by thermal  
neutron flux in nuclear  
research reactors

# $\beta$ decay

- $\beta^-$  decay: proton (quarks: u, u, d)  $\rightarrow$  neutron (quarks: u, d, d)
- $\beta^+$  decay: neutron (quarks: u, d, d)  $\rightarrow$  proton (quarks: u, u, d)

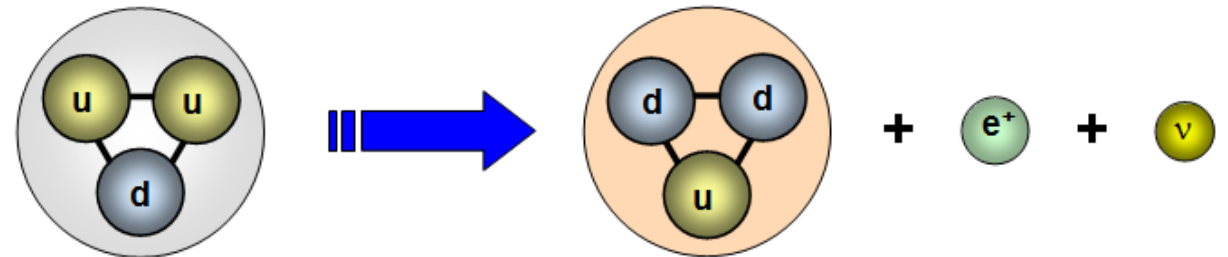
## Quarks



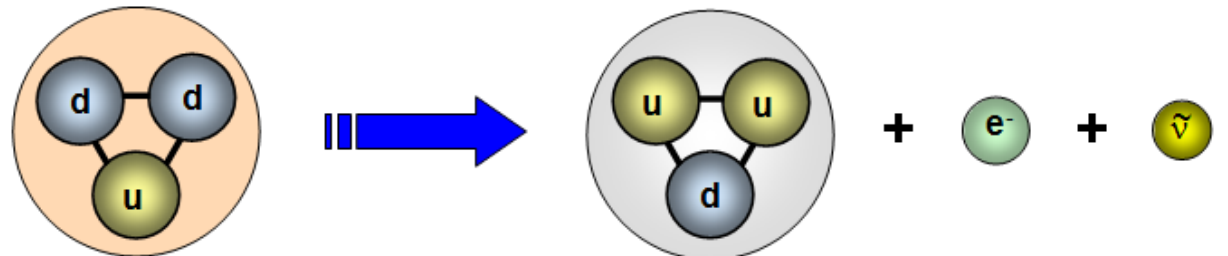
$$\text{Proton} = u u d = +\frac{2}{3} + \frac{2}{3} - \frac{1}{3} = +1$$

$$\text{Neutron} = u d d = +\frac{2}{3} - \frac{1}{3} - \frac{1}{3} = 0$$

Beta<sup>+</sup> decay:  $p \rightarrow n + \beta^+ + \nu$

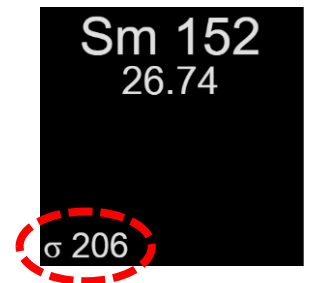


Beta<sup>-</sup> decay:  $n \rightarrow p + \beta^- + \bar{\nu}$



# Neutron – nucleus interactions

- 3 main types
  - Elastic collisions = scattering (billiard ball interactions) → Moderation (slowing down neutrons)
  - Neutron absorption
    - Nuclear fission → Nuclear chain reaction (splitting of atoms)
    - Nuclear transmutation → Isotope production
- Nuclear cross section → Describes probability of a nuclear reaction to occur → characteristic area
  - Higher nuclear cross section => higher probability of interaction
  - Expressed in barn ( $10^{-24} \text{ cm}^2$ )
- Thermal neutrons → Larger probability of interaction
  - Larger effective neutron absorption cross-section
  - Can be absorbed more easily by an atomic nucleus
  - Creates more heavy isotope of the same chemical element (often unstable)

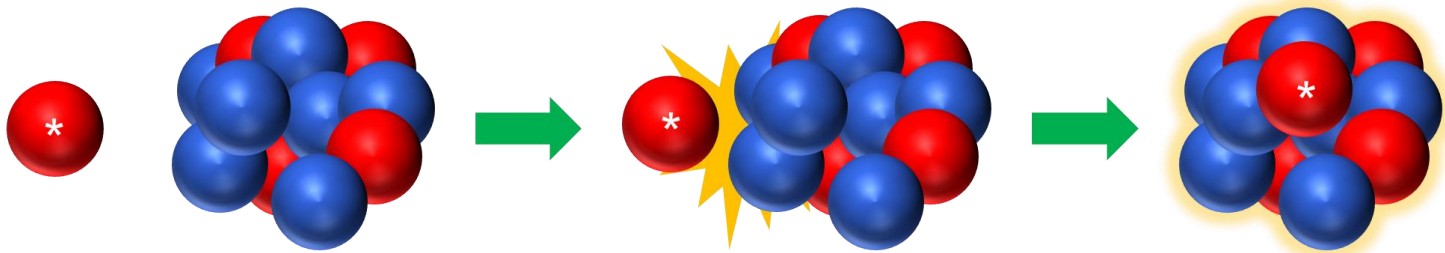


## NEUTRON ACTIVATION

# Neutron activation

Process where neutron radiation induces radioactivity in materials

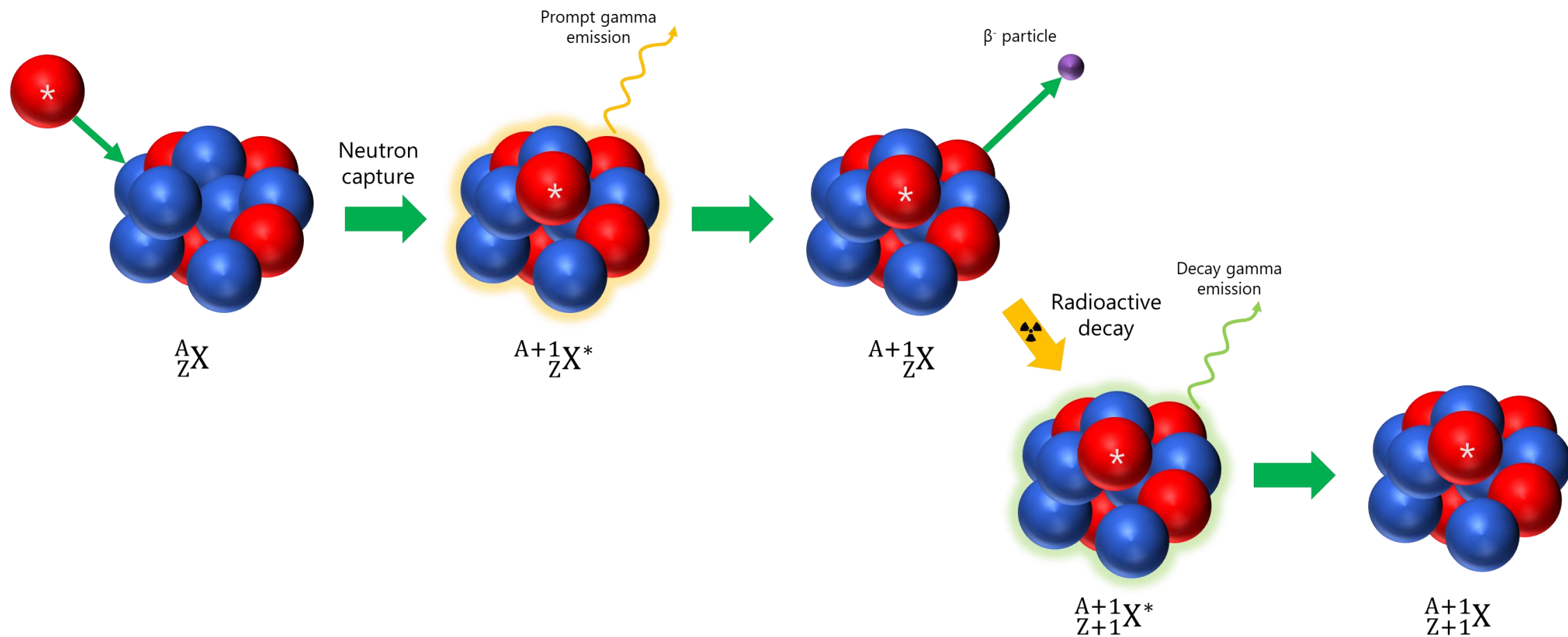
- Atomic target nucleus captures free neutron, becoming heavier and entering excited state
- Immediately followed by gamma emission (photon) → (n,γ) reaction
- Typically yields an unstable (i.e. radioactive) activation product
  - Emits particles to become stable again → electrons ( $\beta^-$ ),  $^4\text{He}$  ( $\alpha$ ), neutrons, fission products
  - Half-lives range from fractions of a second till many thousands of years
- Production of neutron-rich isotopes



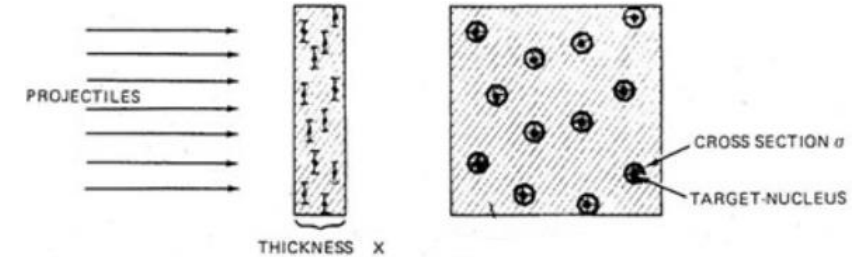
Sm 152	Sm 153
26.74	46.284 h
	(n,γ)
	β <sup>-</sup> 0.7, 0.8...
	γ 103, 70..., e <sup>-</sup>
σ 206	σ 420



# Neutron activation



# Neutron activation *(simplified)*



$$A = A_0 \cdot e^{-\lambda \cdot t}$$

$$A = N_{\text{target}} \cdot \chi_{\text{target}} \cdot \sigma_{\text{target}} \cdot \Phi_{\text{reactor}} \cdot (1 - e^{-\lambda_{\text{isotope}} \cdot t_{\text{irradiation}}})$$

- $A_{\text{isotope}}$  = activity of isotope ( $\text{Bq} = \text{s}^{-1}$ )
- $N_{\text{target}}$  = number of particles in target
- $\chi_{\text{target}}$  = isotopic and chemical purity of the target (enrichment)
- $\sigma_{\text{th, target}}$  = cross section of target for neutrons ( $\text{barn} = 10^{-24} \text{ cm}^2$ )
- $\Phi_{\text{reactor}}$  = neutron flux ( $\text{neutrons/cm}^2/\text{s}$ )
- $\lambda_{\text{isotope}}$  = radioactive decay constant of produced radionuclide ( $\text{s}^{-1}$ )  
 $= \ln(2) / t_{1/2, \text{isotope}}$
- $t_{\text{irradiation}}$  = target irradiation time (s)

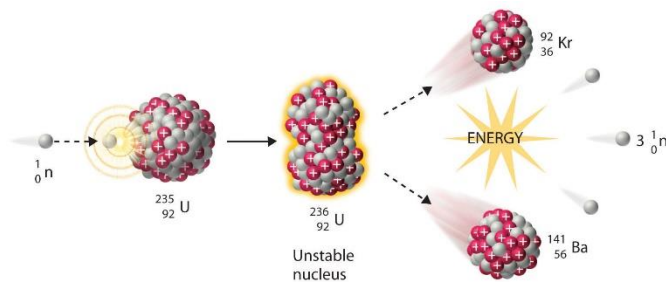
## Not considered

- Self-shielding in the target
- Flux variations
- Burn-up of the target material with time
- Subsequent neutron capture

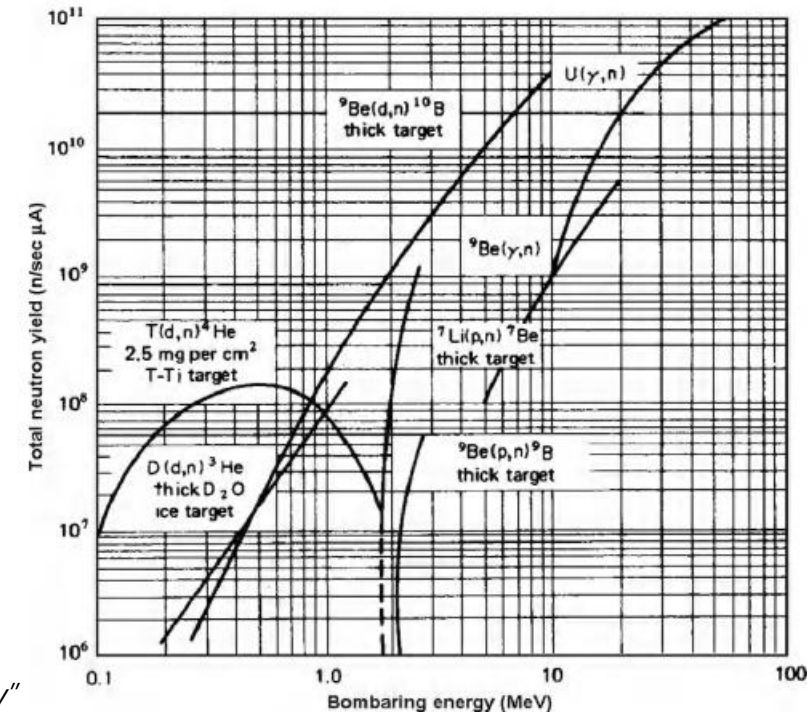
# Neutron source

Production of neutron-rich radionuclides require neutrons

- Neutrons are bound to a nucleus, and do not exist free for long in nature
- Neutron source needed
  - Nuclear fission
  - Nuclear reactions induced by radioisotopes
  - Accelerator-induced reaction



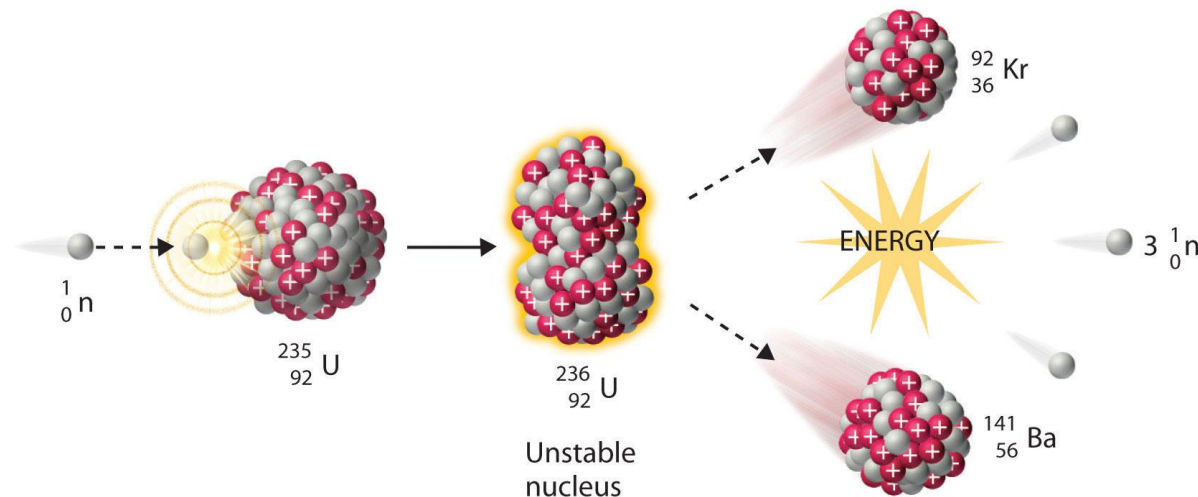
Material	Half-life	Neutron yield ( $\text{n s}^{-1} \text{ Bq}^{-1}$ )	$\gamma$ -dose rate <sup>(a)</sup> ( $\text{mSv h}^{-1} \text{ m}^2 \text{ Bq}^{-1}$ )
$^{226}\text{Ra} + \text{Be}$	1600 y	$3.5 \times 10^{-4}$	850
$^{239}\text{Pu} + \text{Be}$	24110 y	$2.4 \times 10^{-4}$	4
$^{239}\text{Pu} + ^{18}\text{O}$	24110 y	$7.8 \times 10^{-6}$	(b)
$^{241}\text{Am} + \text{Be}$	433 y	$6.8 \times 10^{-5}$	2.5
$^{210}\text{Po} + \text{Be}$	138 d	$6.8 \times 10^{-5}$	$< 0.3^{(c)}$
$^{124}\text{Sb} + \text{Be}$	60 d	$\sim 5 \times 10^{-6}$	1000
$^{252}\text{Cf}$	2.6 y	$5 \times 10^{12} \text{ n s}^{-1} \text{ g}^{-1}$	(d)



# Neutron source – Fission

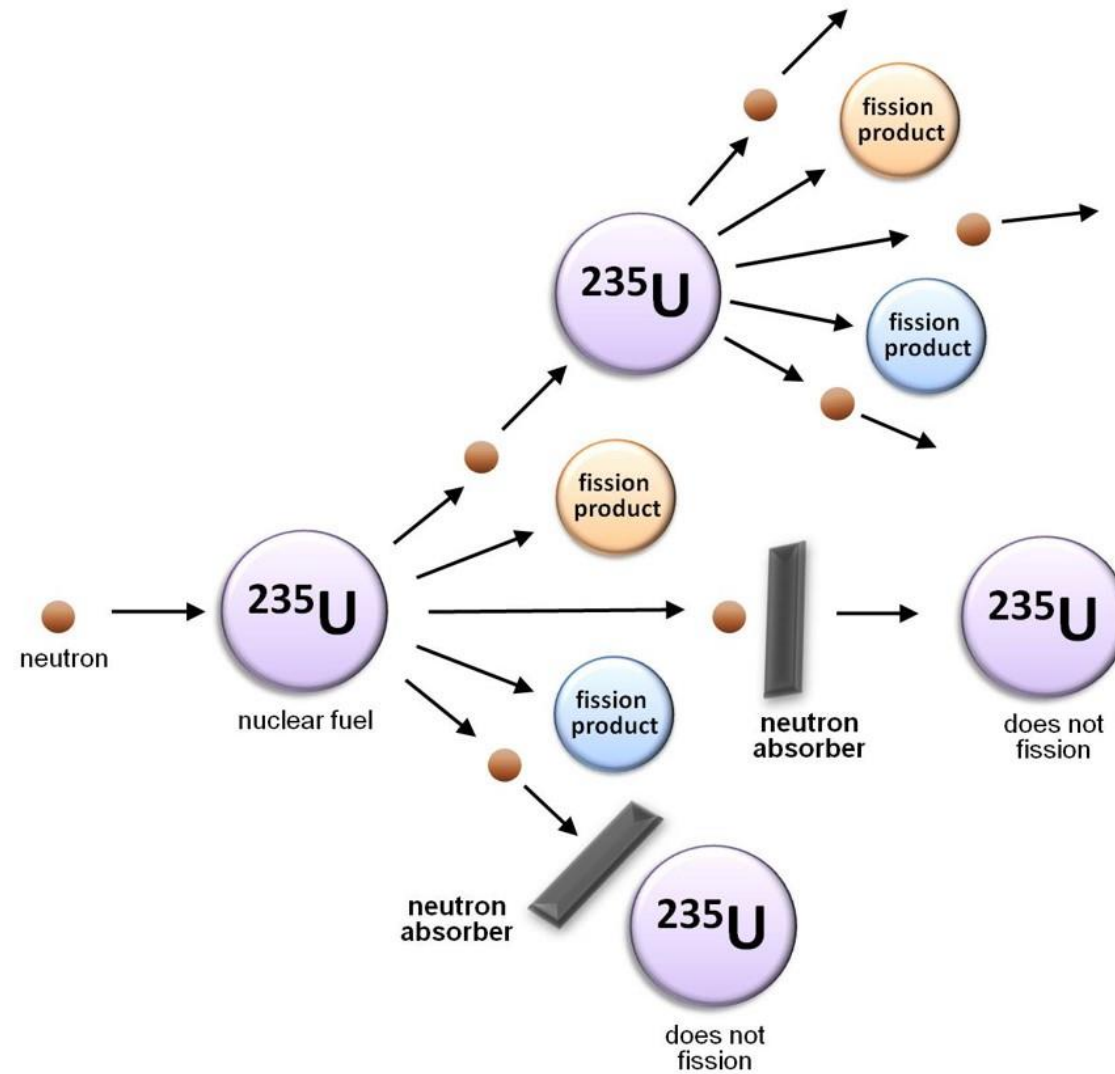
Nuclear fission  $^{235}\text{U}(\text{n},\text{f})$  yields fission products +  $\pm 2.5 \text{ n}^0$  + energy (ca. 200 MeV)

- Highly efficient neutron source
- Nuclear chain reaction → needs to be controlled once critical
- Takes place in a nuclear reactor

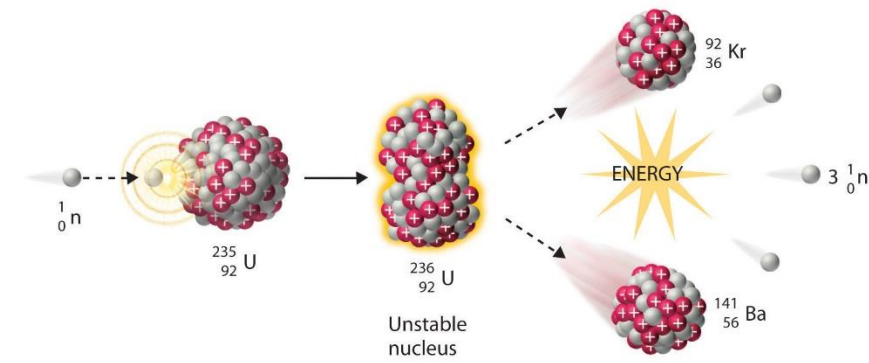




# Neutron source

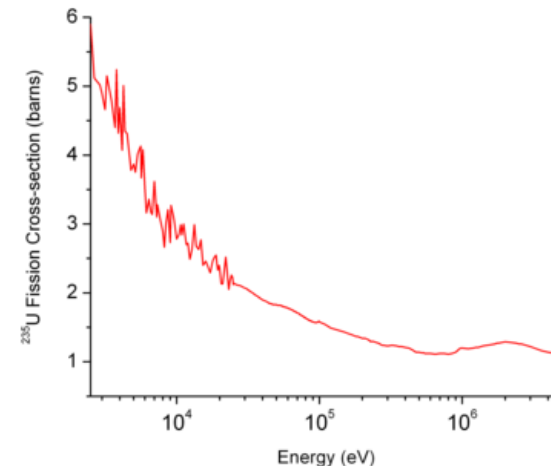
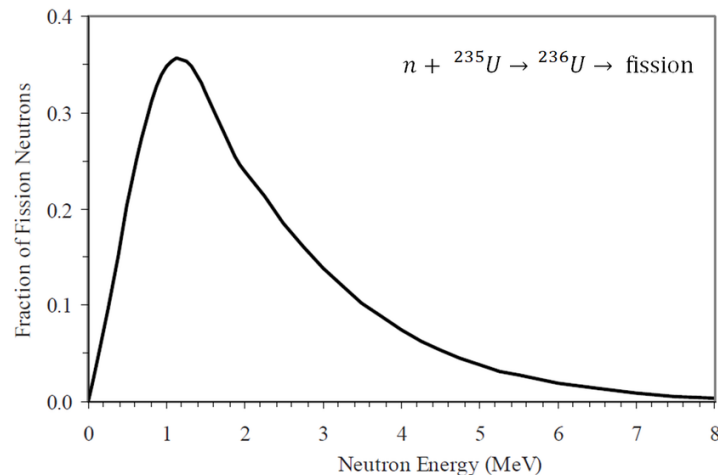


# Neutron energy

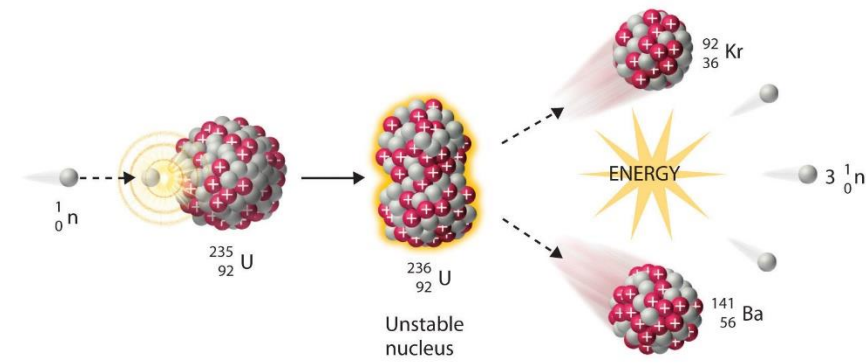


$^{235}\text{U}(n,f) \rightarrow$  Unstable  $^{236}\text{U}$  nucleus 'explodes', ejecting fission products and neutrons at high kinetic energy and velocity

- Release of neutrons from nucleus requires exceeding binding energy (7-9 MeV)
- 'Fast neutrons' – 1-20 MeV, traveling ca 20,000 km/s
- Low probability of being captured by  $^{235}\text{U}$  atoms (or other target atoms)
- Not very suitable for maintaining fission reaction or radionuclide production



# Neutron energy

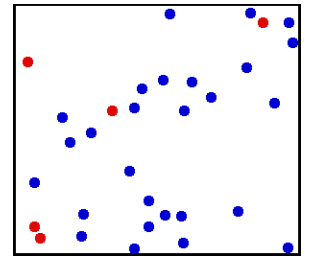
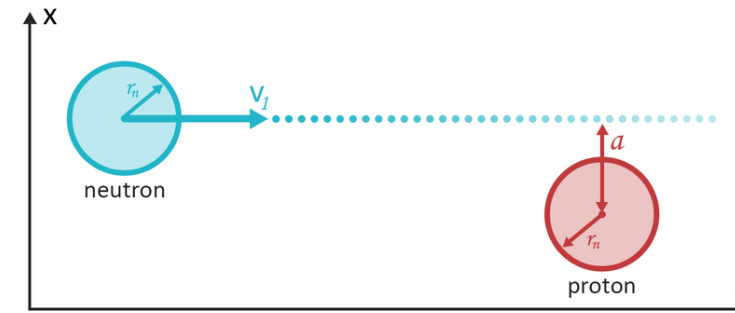


${}^{235}\text{U}(\text{n},\text{f}) \rightarrow$  Unstable  ${}^{236}\text{U}$  nucleus 'explodes', ejecting fission products and neutrons at high kinetic energy and velocity

- Release of neutrons from nucleus requires exceeding binding energy (7-9 MeV)
- 'Fast neutrons' – 1-20 MeV, traveling ca 20,000 km/s
- Low probability of being captured by  ${}^{235}\text{U}$  atoms (or other target atoms)
- Not very suitable for maintaining fission reaction or radionuclide production
- **Neutrons must be slowed down without being captured**
- Transfer of energy to a moderator

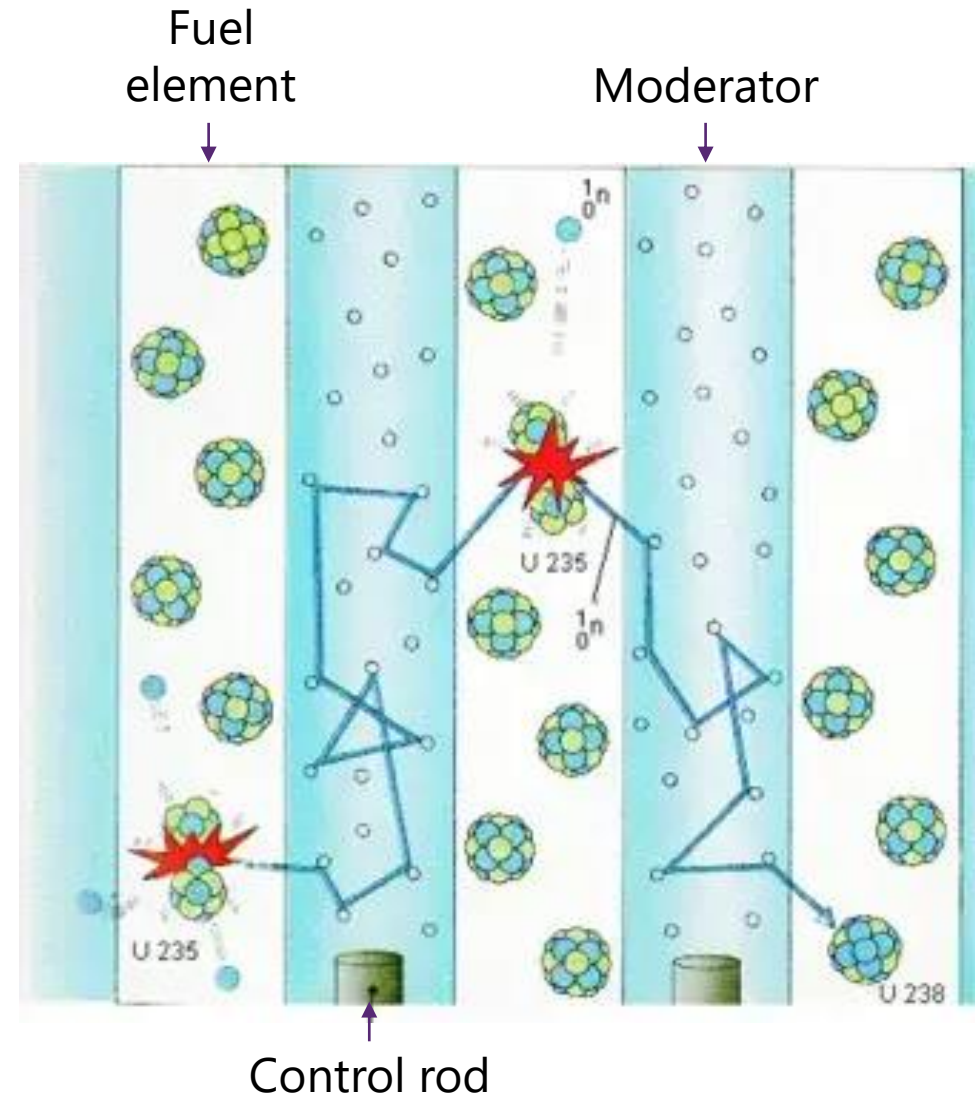
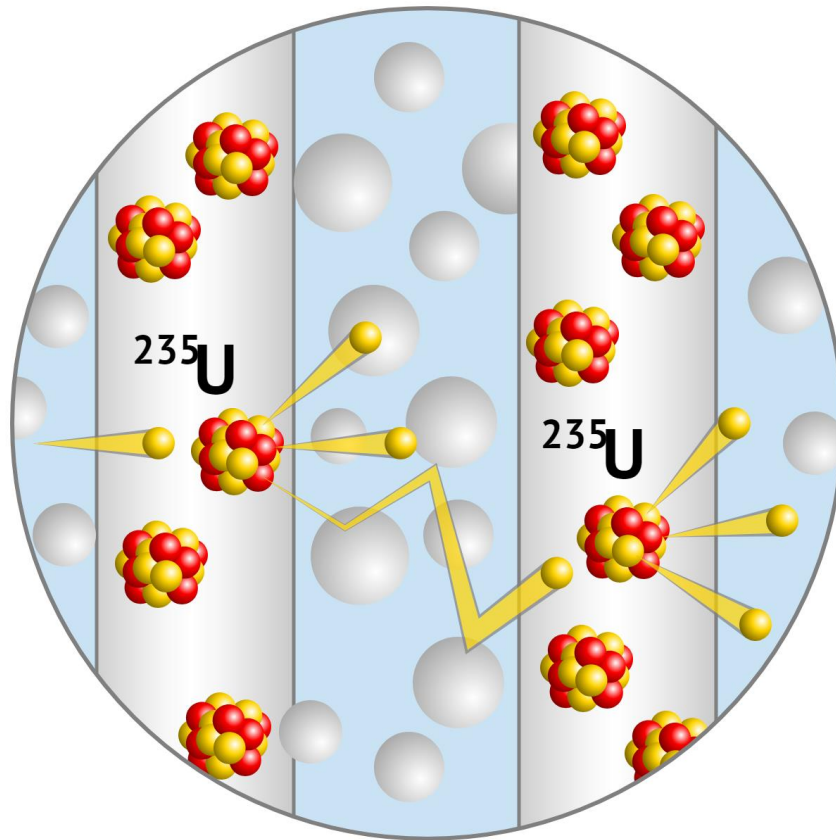
# Neutron energy

- **Neutron moderation** → Reduction of the initial high speed, i.e. high kinetic energy, of the free neutron
- Conservation of energy → reduction of energy = transfer of energy to another material, i.e. the moderator (= the medium)
- Performed by a large number of successive collisions with a material that scatters strongly, but absorbs weakly → High neutron scatter cross section
  - Energy is predominantly transferred by elastic collisions
  - Most efficient removal of  $E_{k,n}$  by moderating nucleus with near-identical mass
  - $^1\text{H}$  is an almost perfect choice ( $m_p \approx m_n$ )
  - Maxwell-Boltzmann distribution of  $E_k$
  - $\text{H}_2\text{O}$ ,  $\text{D}_2\text{O}$ , graphite, Be





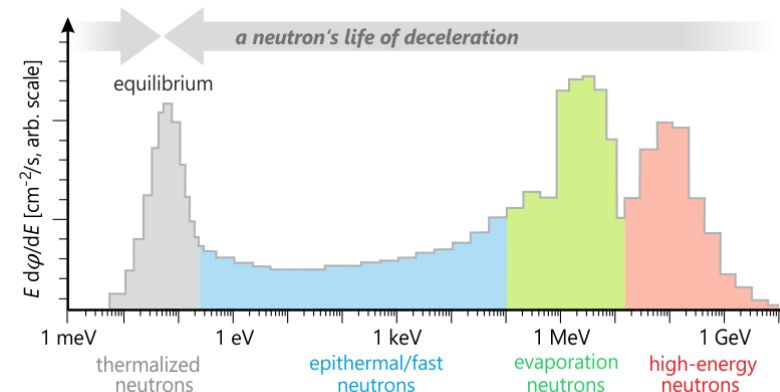
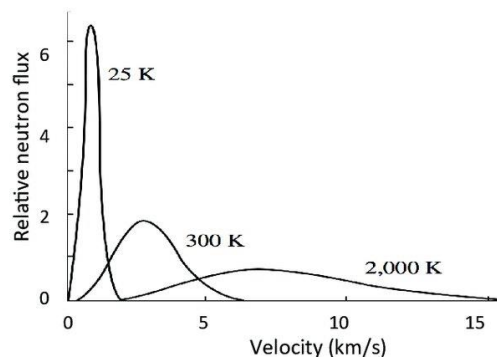
# Neutron energy



# Neutron energy

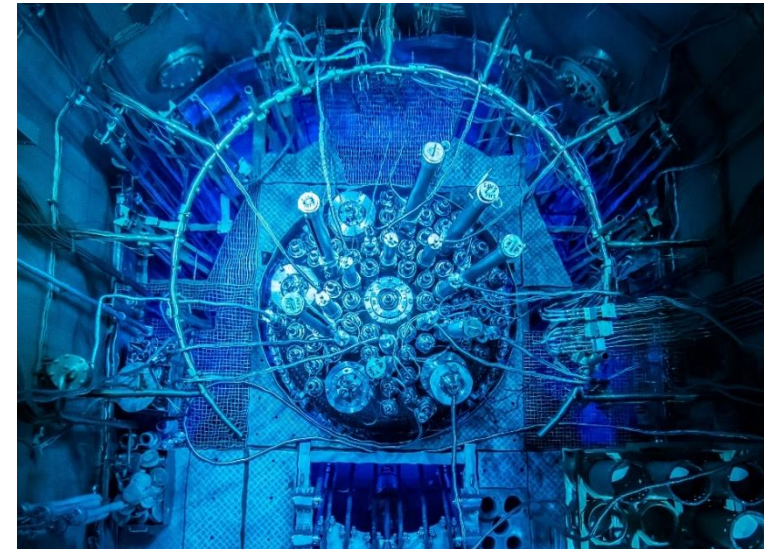
‘Neutron temperature’ → indicates a free neutron’s kinetic energy (eV)

- $\bar{E} = \frac{1}{2} m_n \langle v_n^2 \rangle = \frac{3}{2} k_B T$   
 $m_n$  = the neutron mass  
 $v_n^2$  = the average squared neutron speed  
 $k_B$  = Boltzmann constant (1.38E-23 J/K = 8.62E-5 eV/K)
- 1 MeV →  $T \approx 7.7\text{E}9$  K (thermodynamic temperature)
- Fast neutron: 1 – 20 MeV → 7.7 – 154 billion K → ‘Hot neutrons’
- Neutron energy comparable to energy of surrounding particles → ‘Thermalized’
  - Thermal neutrons ( $\approx 0.025$  eV, traveling at 2.2 km/s)
  - Energy corresponding to most probable speed at 300 K (H<sub>2</sub>O medium in water tank)



# Research reactors

- Developed and designed for material testing
  - Purpose = neutron flux irradiations and impact studies
  - Powerful high flux neutron source → 'Neutron factory'
  - Not for electricity production → All produced heat is evacuated by cooling water = by-product
- Allow for ease of access to neutrons
  - Access during operation
  - Shielding compatible with installation of experimental devices
- Provide flexibility in utilization
  - Configuration and operation parameters can be varied



# Research reactors

## NDA

---

### III. INTRODUCTION

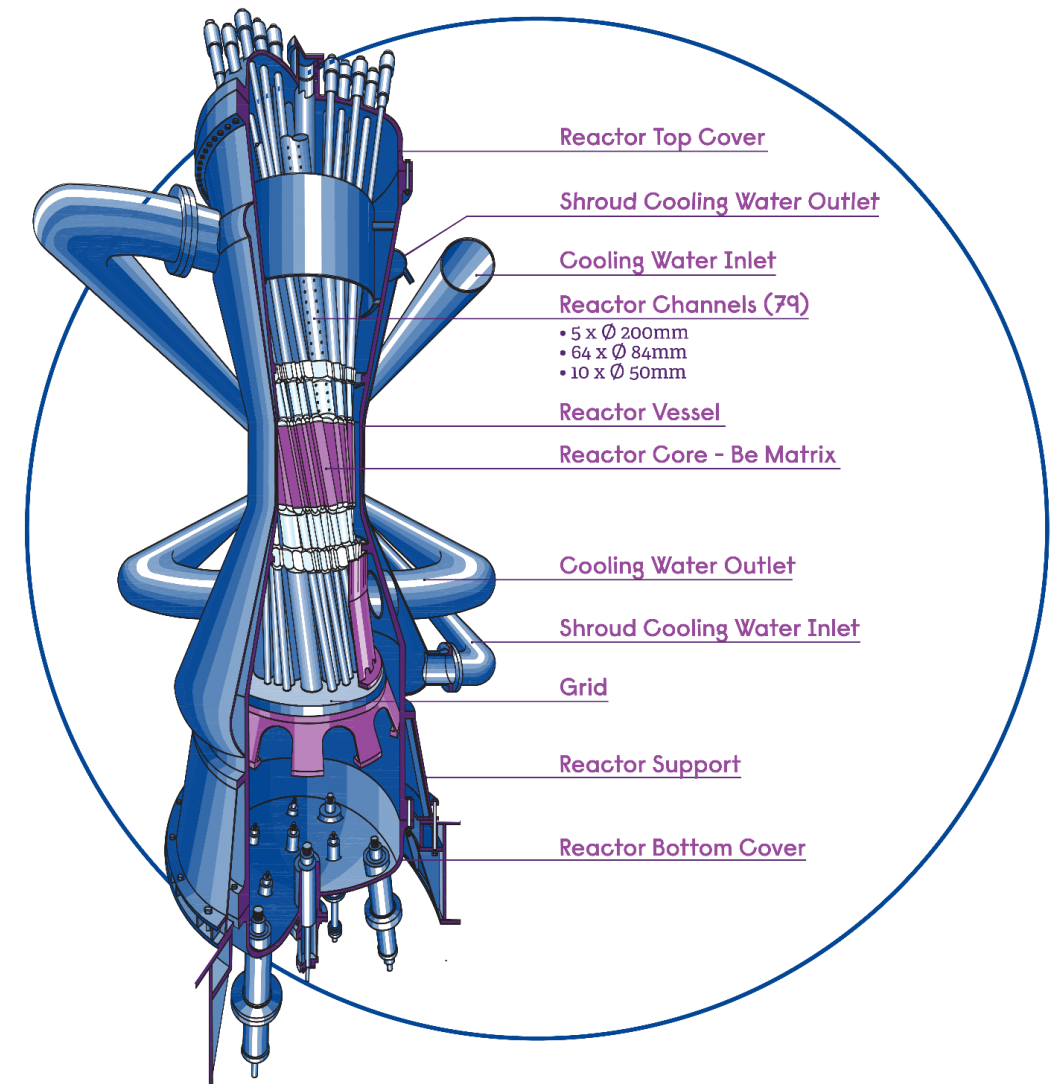
#### A. PURPOSE OF PROJECT AND PHASE I

Under terms of a contract with the Centre d'Etudes pour les Applications de l'Energie Nucleaire (CEAN), the Nuclear Development Corporation of America (NDA) undertook the design of an engineering test reactor for Belgium. This reactor is intended to provide CEAN with a test facility of greatest overall usefulness in a future power reactor development program. Inasmuch as the present CEAN graphite reactor, BR I, already provides low neutron flux facilities, a basic objective of this program was to provide high flux test facilities of ready accessibility.

# Research reactors

Flux results from power and size

- Thermal spectrum most favorable
  1. Compact design
  2. Water cooling
  3. Metallic
- Pool type reactors allow for
  - Easy access
  - Shielding
  - Heat sink
- Large (= high power) reactors allow wider range of conditions
  - Flux ranges and reactivity variation
  - More flexible core configuration

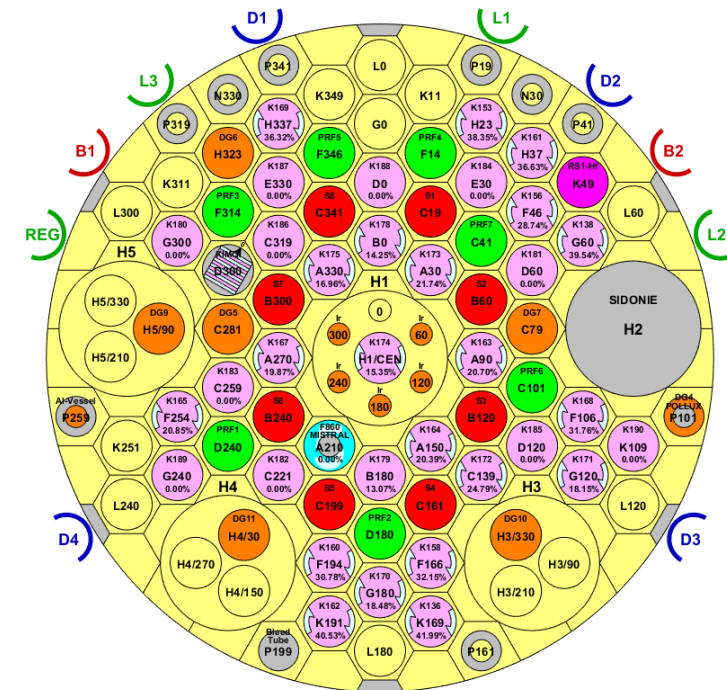
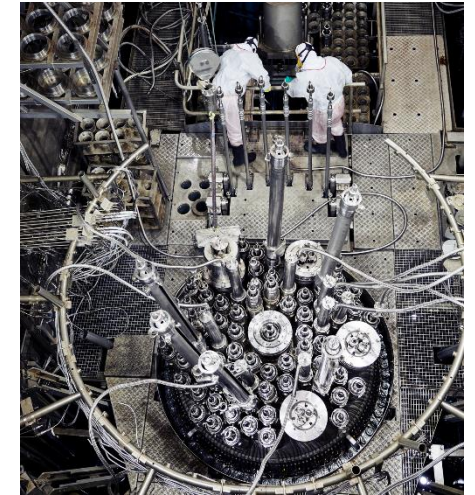
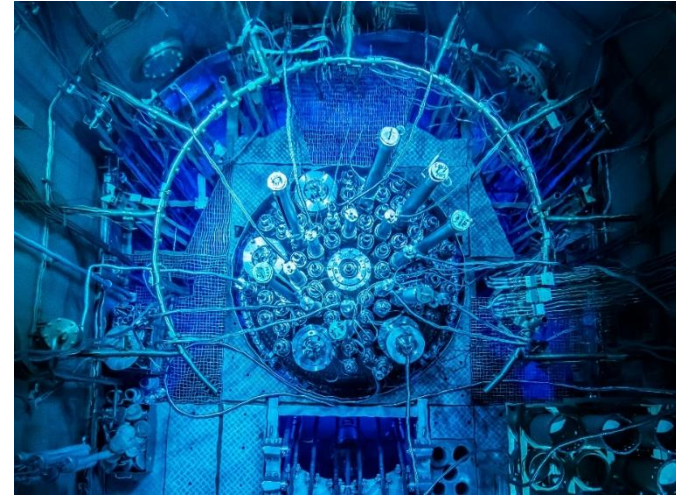




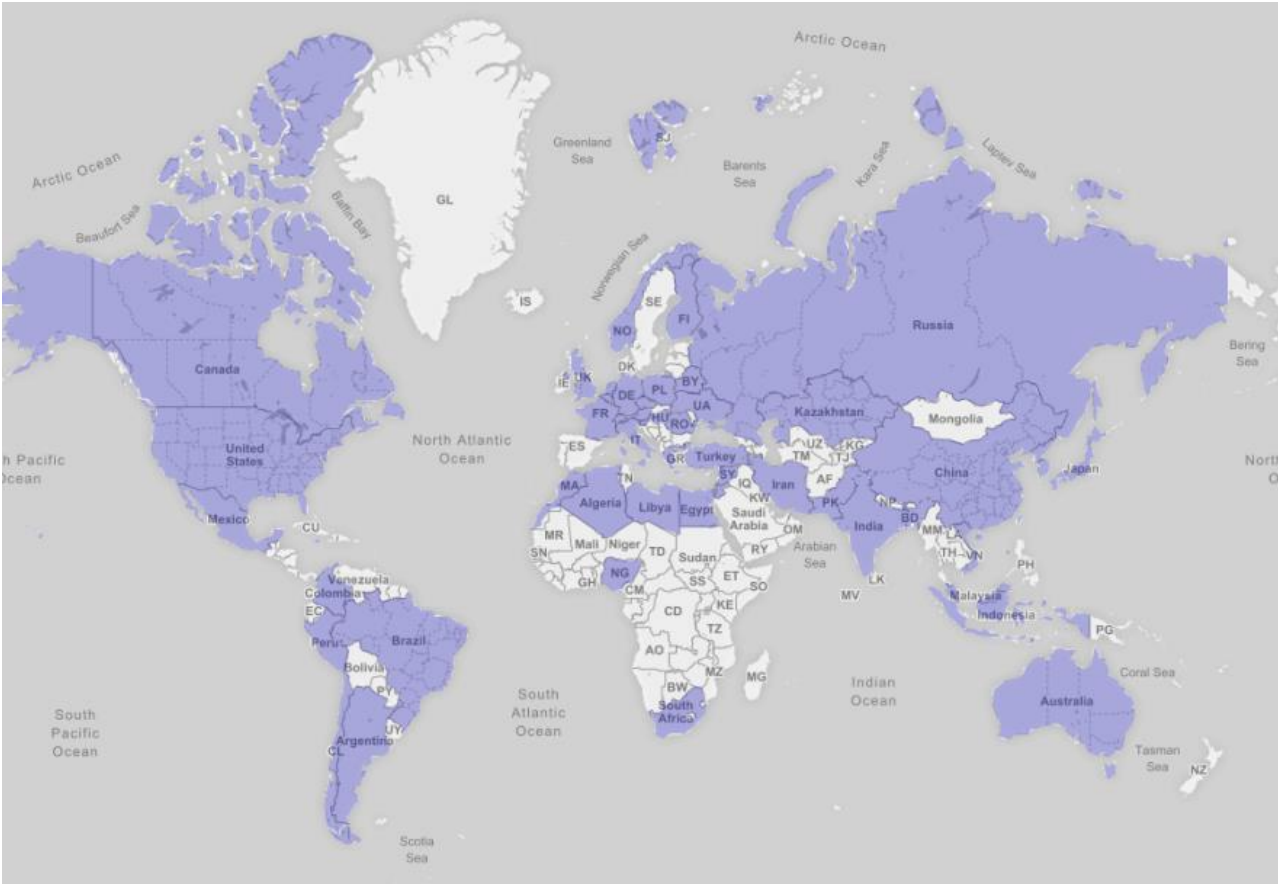
# Research reactors

Flux results from power and size

- Thermal spectrum most favorable
  1. Compact design
  2. Water cooling
  3. Metallic
- Pool type reactors allow for
  - Easy access
  - Shielding
  - Heat sink
- Large (= high power) reactors allow wider range of conditions
  - Flux ranges and reactivity variation
  - More flexible core configuration



# Research reactors available



Total  
**840** Reactors  
in 70 countries



Operational  
**226** Reactors  
in 54 countries

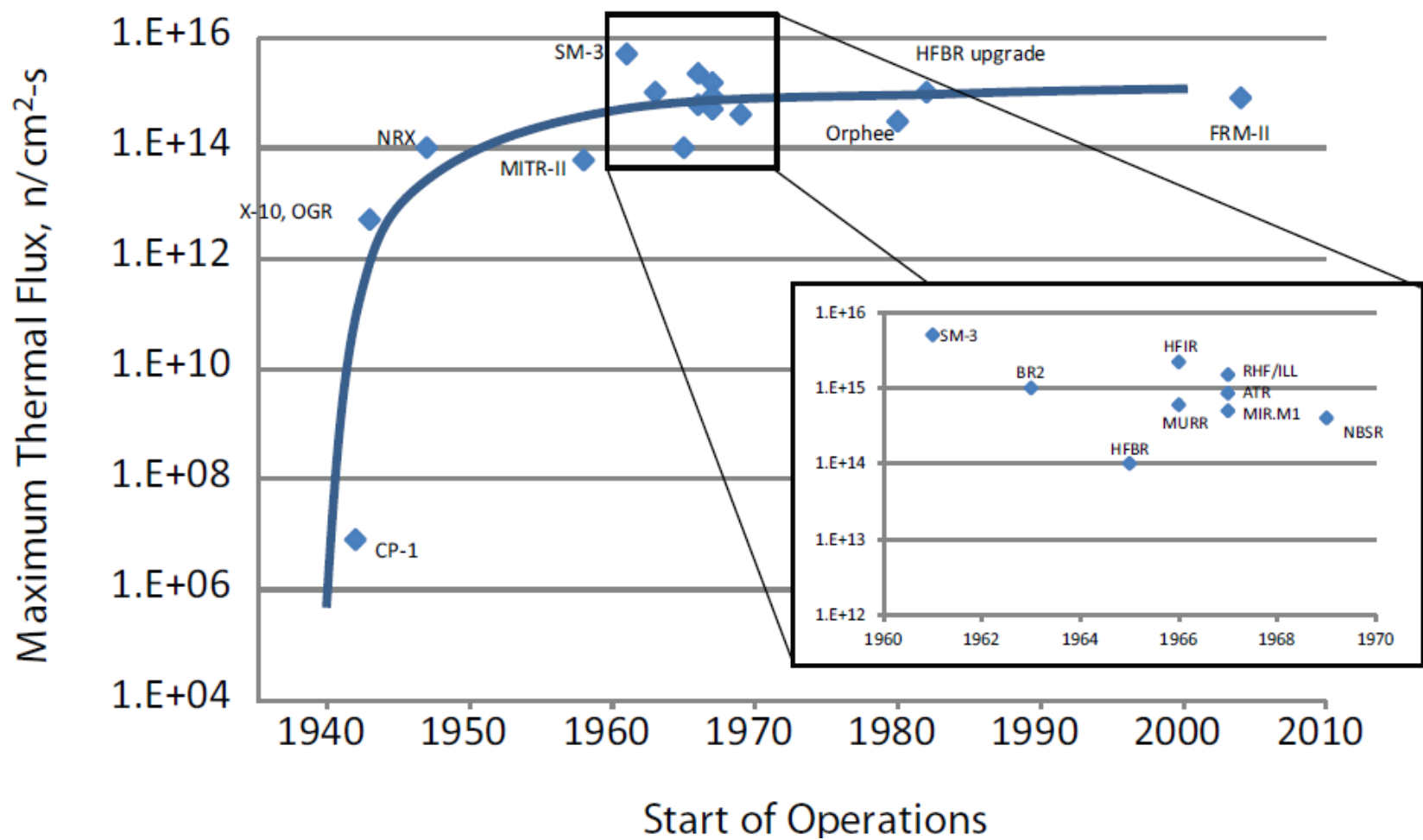


**81** are utilized for Isotope production

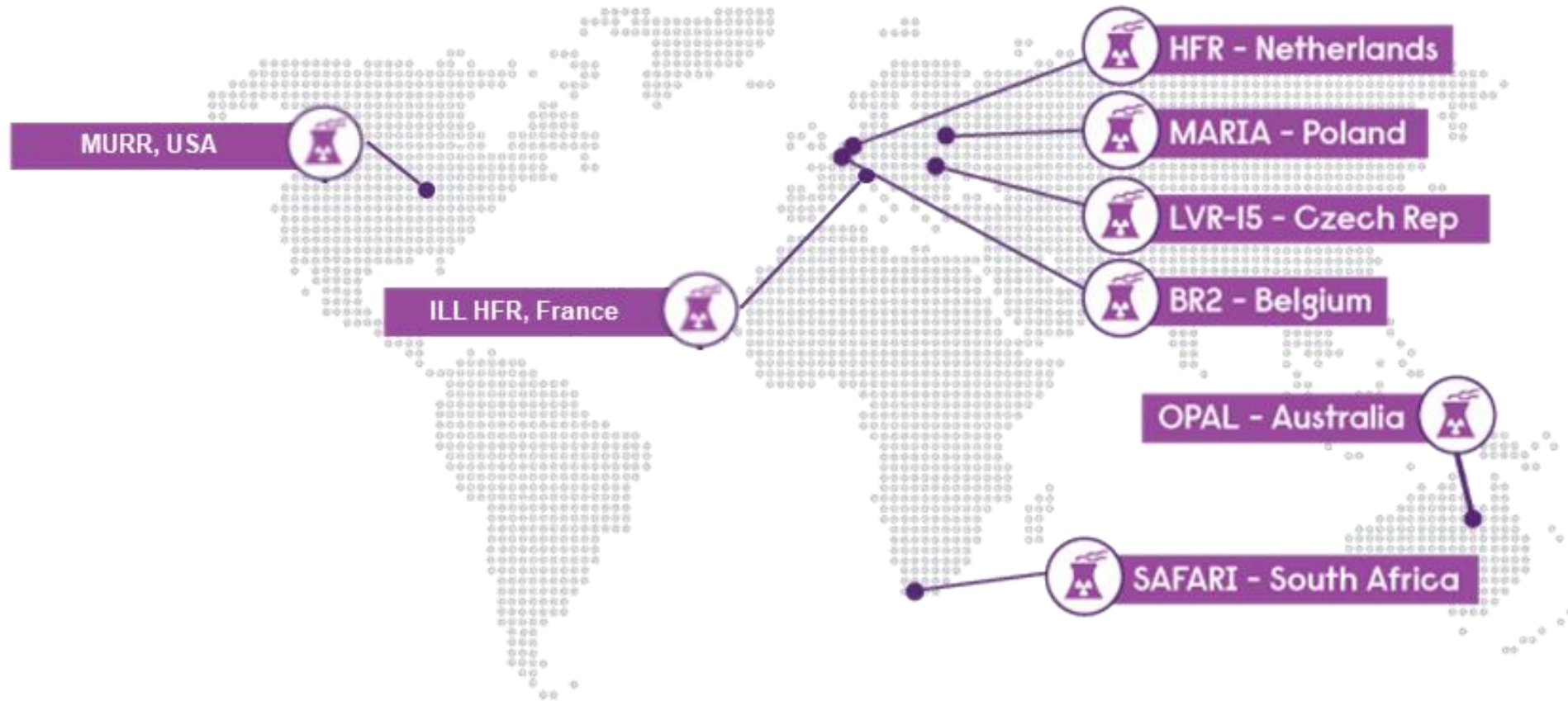
Under construction/Planned  
**20** Reactors  
in 15 countries



# Research reactors

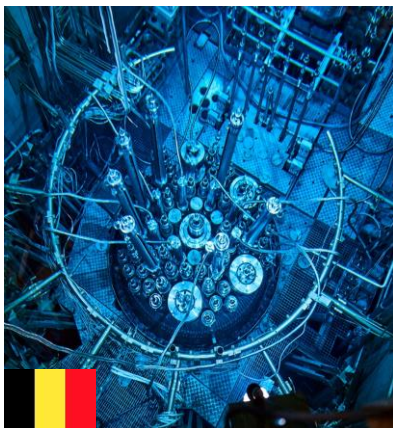


# Research reactors



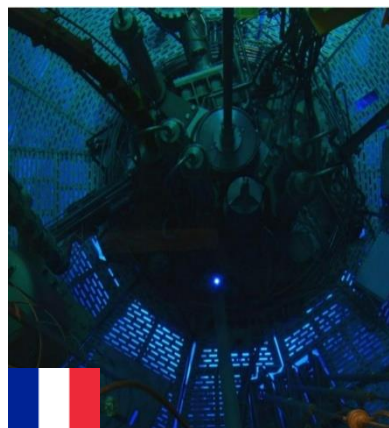


# Research reactors *(current capacity in EU)*



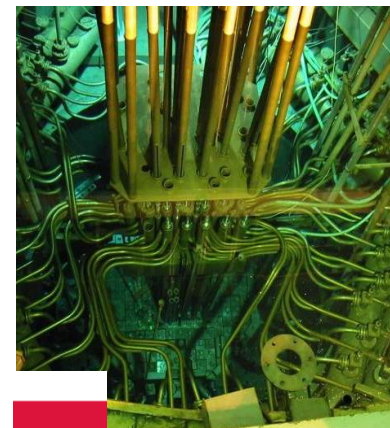
**BR2 – SCK CEN**

$\phi_{th}$  up to  $4 \times 10^{14}$  neutrons/cm<sup>2</sup>/s (flexible)  
 $1 \times 10^{15}$  neutrons/cm<sup>2</sup>/s (pressure vessel)



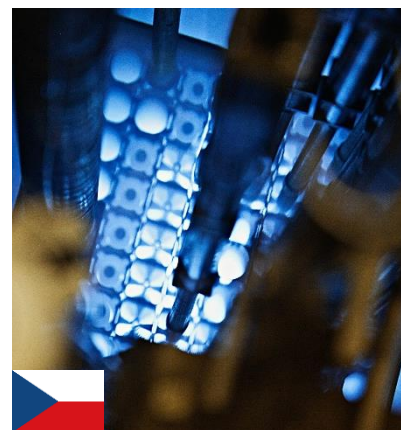
**RHF – ILL**

$\Phi_{th}$  up to  $1.5 \times 10^{15}$  neutrons/cm<sup>2</sup>/s



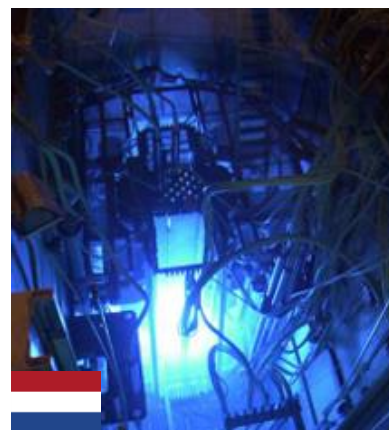
**MARIA – Polatom**

$\Phi_{th}$  up to  $3 \times 10^{14}$  neutrons/cm<sup>2</sup>/s



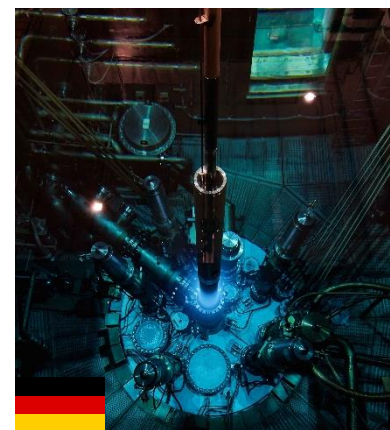
**LVR-15 – CICRR**

$\phi_{th}$  up to  $1 \times 10^{14}$  neutrons/cm<sup>2</sup>/s



**HFR - NRG**

$\phi_{th}$  up to  $2.6 \times 10^{14}$  neutrons/cm<sup>2</sup>/s



**FRM II - TUM**

$\phi_{th}$  up to  $1.3 \times 10^{14}$  neutrons/cm<sup>2</sup>/s





# Research reactors *(future capacity in EU)*



**JHR – CEA**  
Operational: ca. 2032



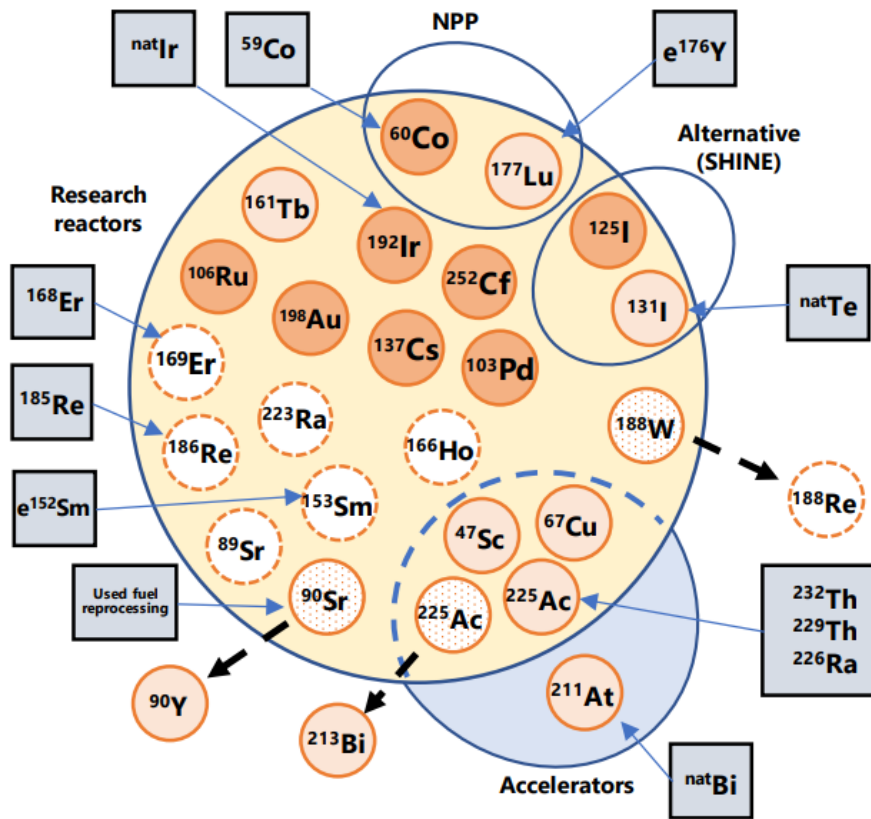
**PALLAS - NRG**  
Operational: ca. 2030

# Potential difficulties

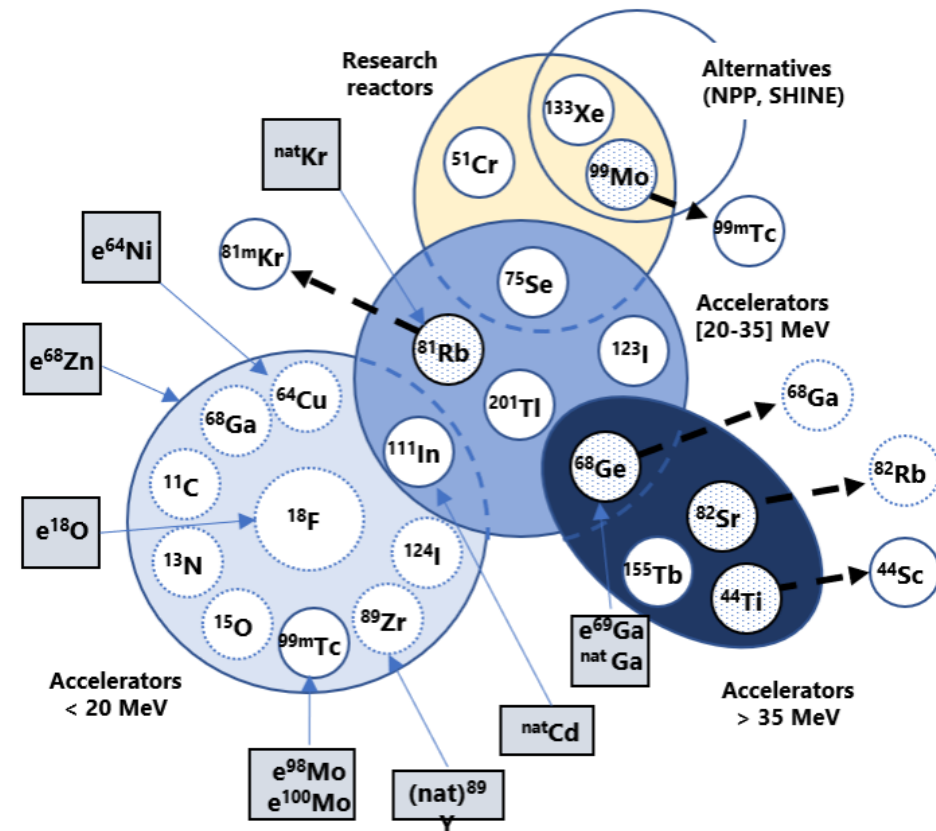
- Proliferation of fissile material → Conversion to LEU (< 20%  $^{235}\text{U}$  enrichment)
- Ageing research reactor fleet → Most reactors were constructed in 1960s
- Strong support by public subsidies
- Operation cycles altered with maintenance cycles
- Severe safety measurements
- Current research reactors were designed and optimized for material testing, not for medical radionuclide production
- Irradiation positions are limited, especially the very high flux ones
  - High demand = high competitions = increasing prices
  - Find alternative high thermal neutron sources (e.g. CANDU commercial power reactors)

	Nuclear reactors	Cyclotrons
<b>Principle of production</b>	Target material inserted in the neutron flux field undergoes fission or neutron activation transmuting into radionuclide of interest	Target material irradiation by charged particle beams. Including nuclear reactions that transmute the material into radionuclide of interest
<b>Transmutation base</b>	Neutrons	p, d, t, $^3\text{He}$ , $\alpha$ or heavy ion beams
<b>Advantages</b>	<ul style="list-style-type: none"> <li>Production of neutron rich radionuclides, mostly for <b>therapeutic use</b></li> <li>High production yield and production efficiency</li> <li>Centralized production: one research reactor able to supply to large regions, in some cases even globally</li> </ul>	<ul style="list-style-type: none"> <li>Production of proton rich elements used as <math>\beta^+</math> emitters for PET scans → <b>diagnostic use</b></li> <li>Decentralized production allows for back-up chains</li> <li>High up-time</li> <li>High specific activity in most cases</li> <li>Small initial investment in comparison to nuclear reactor</li> <li>Little long-lived radioactive waste</li> </ul>
<b>Disadvantages</b>	<ul style="list-style-type: none"> <li>Extremely high initial investment cost</li> <li>High operational costs</li> <li>Considerable amounts of long-lived radioactive waste</li> <li>Long out-of-service periods</li> <li>Trouble to back-up in case of unforeseen downtime</li> <li>Demanding logistics, often involving air transport</li> <li>Public safety concerns</li> <li>Non-proliferation treaty concerns → <b>Conversion to LEU</b></li> </ul>	<ul style="list-style-type: none"> <li>Regional network of cyclotrons and complex logistics needed for short-lived produced radionuclides</li> <li>Radionuclide production limited depending on installed beam energy</li> <li>Lower production yield</li> </ul>

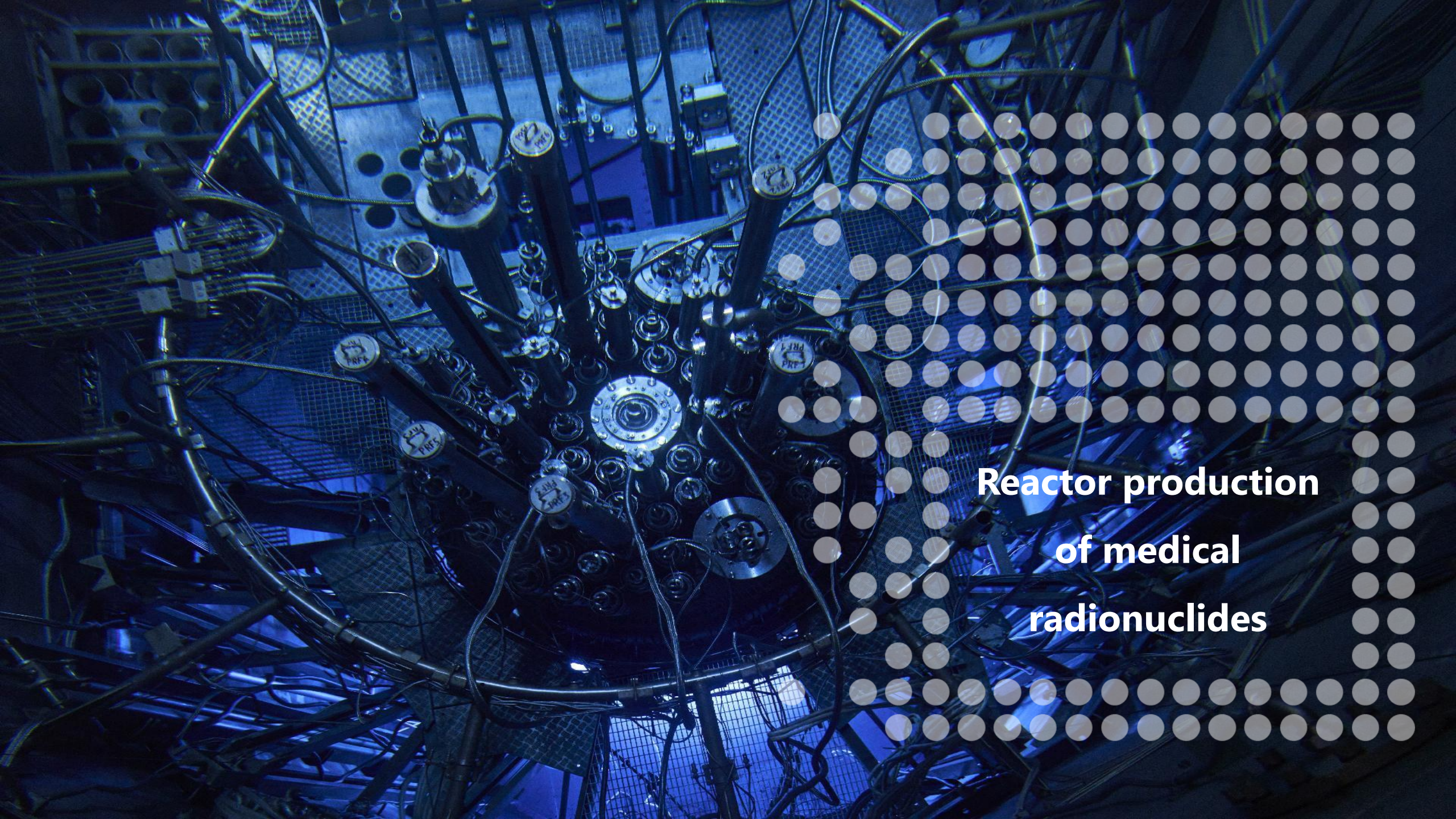
# Therapeutic radionuclides



## Diagnostic radionuclides





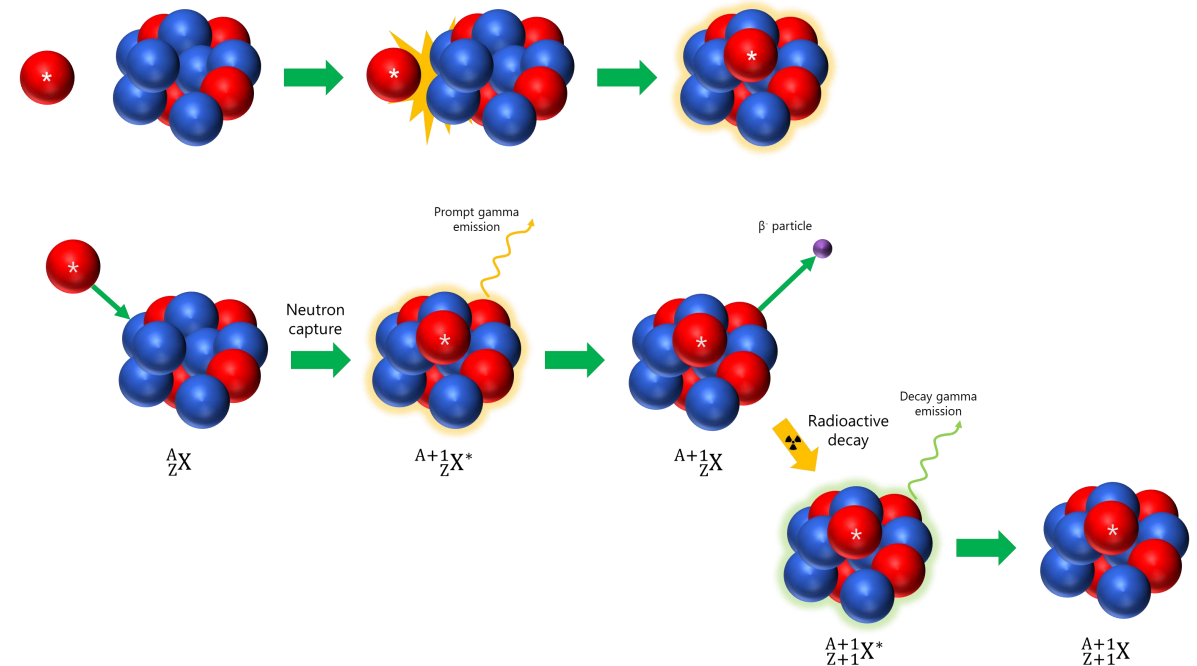
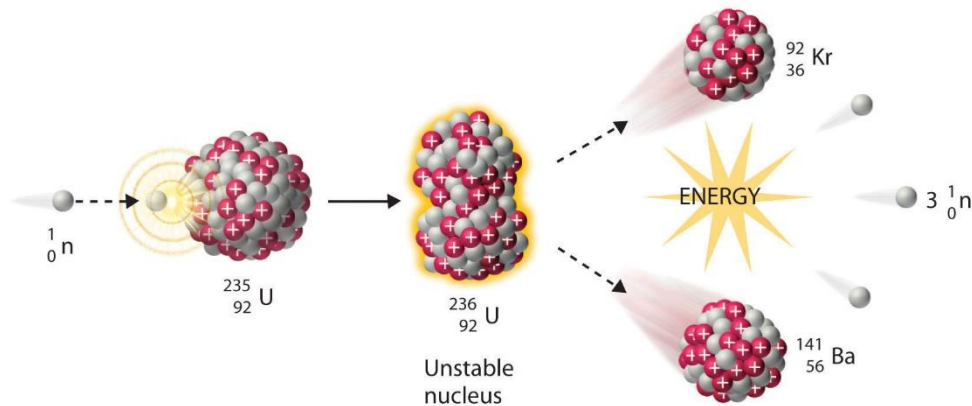


**Reactor production  
of medical  
radionuclides**



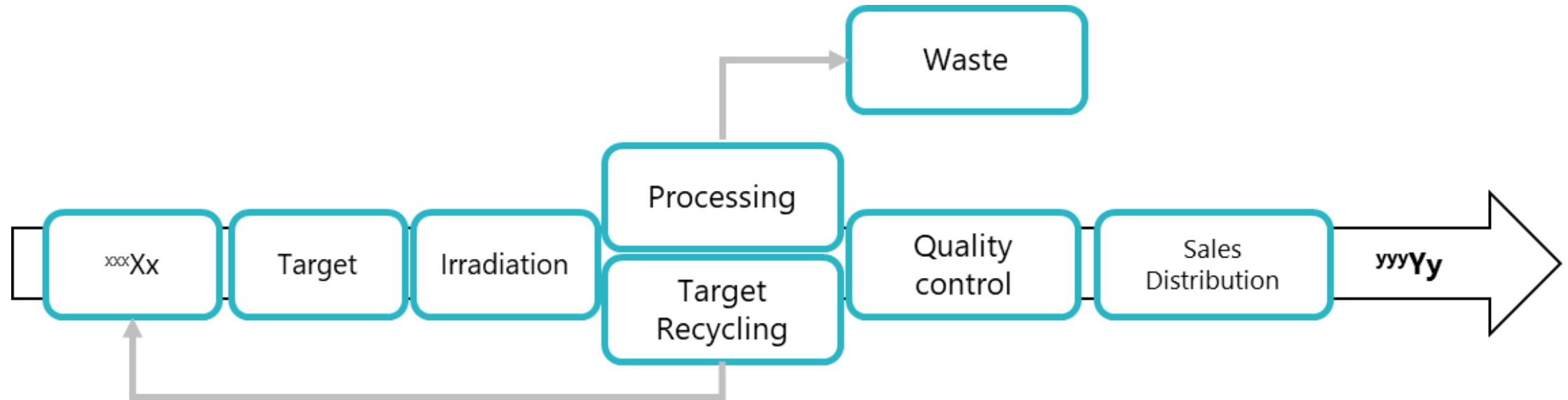
# Production strategies

1. Fission  $^{235}\text{U}(\text{n},\text{f})$
2. Neutron activation ( $\text{n},\gamma$ ) of highly enriched targets
  - Carrier added
  - Non-carrier added





# Production strategies



Radionuclide	Half life	Application	Production method
$^{99}\text{Mo}/^{99\text{m}}\text{Tc}$	66 h/6 h	SPECT	$^{235}\text{U}$ fission $^{98}\text{Mo}(n,\gamma)^{99}\text{Mo}$
$^{131}\text{I}$	8 d	Radionuclide therapy	$^{235}\text{U}$ fission $^{130}\text{Te}(n,\gamma)^{131}\text{Te} \rightarrow ^{131}\text{I}$
$^{51}\text{Cr}$	28 d		$^{50}\text{Cr}(n,\gamma)^{51}\text{Cr}$
$^{153}\text{Sm}$	46 h		$^{152}\text{Sm}(n,\gamma)^{153}\text{Sm}$
$^{161}\text{Tb}$	6.95 d		$^{160}\text{Gd}(n,\gamma)^{161}\text{Gd} \rightarrow ^{161}\text{Tb}$
$^{166}\text{Ho}$	27 h		$^{165}\text{Ho}(n,\gamma)^{166}\text{Ho}$ $^{164}\text{Dy}(2n,\gamma)^{166}\text{Dy} \rightarrow ^{166}\text{Ho}$
$^{177}\text{Lu}$	6.65 d		$^{176}\text{Lu}(n,\gamma)^{177}\text{Lu}$ $^{176}\text{Yb}(n,\gamma)^{177}\text{Yb} \rightarrow ^{177}\text{Lu}$
$^{90}\text{Y}$	64 h		$^{89}\text{Y}(n,\gamma)^{90}\text{Y}$
$^{188}\text{W}/^{188}\text{Re}$	69.8 d/17 h		$^{186}\text{W}(2n,\gamma)^{188}\text{W} \rightarrow ^{188}\text{Re}$
$^{125}\text{I}$	60 d	Brachytherapy	$^{124}\text{Xe}(n,\gamma)^{125\text{m}}\text{Xe} \rightarrow ^{125}\text{I}$
$^{192}\text{Ir}$	74 d		$^{191}\text{Ir}(n,\gamma)^{192}\text{Ir}$

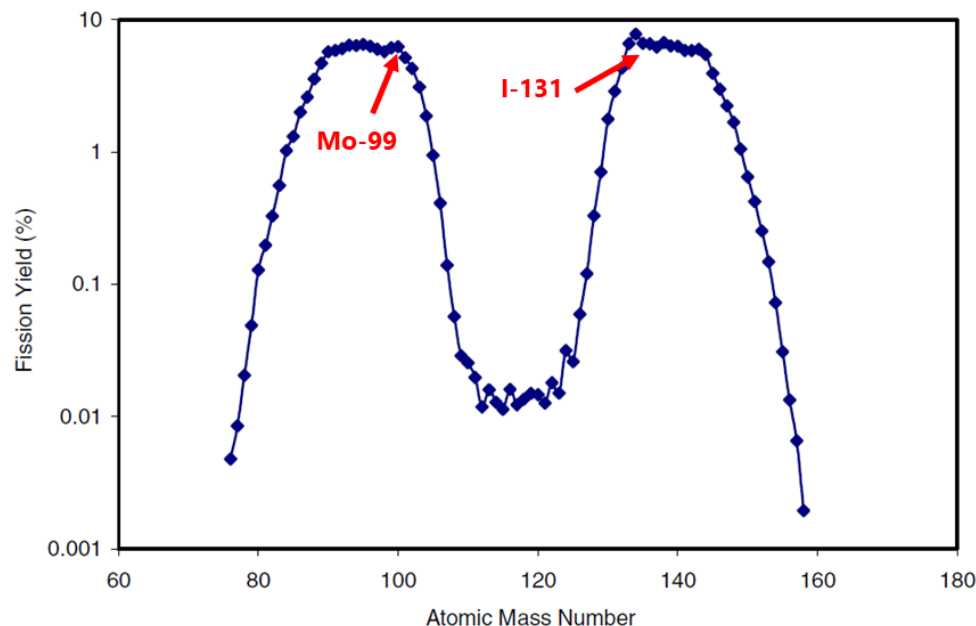
Tc 99	I 131	Xe 133
6.0072 h	8.0252 d	2.198 d
IT (143, 2)		5.2475 d
e <sup>-</sup>	β <sup>-</sup> 0.6, 0.8...	β <sup>-</sup> 0.3...
γ 141	γ 364, 637	γ 81...
β <sup>-</sup> ...	284..., g	e <sup>-</sup>
γ (90...)	σ ~0.7	IT 233, e <sup>-</sup>
σ 22.8		σ 190

# Production strategies – Fission

Fission  $^{235}\text{U}(n,f)$

- Produces wide range of fission products
- Predominant way for  $^{99}\text{Mo}/^{99\text{m}}\text{Tc}$  production,  $^{131}\text{I}$  and  $^{133}\text{Xe}$  are by-products
- Initially by use of HEU (90-95%  $^{235}\text{U}$ ), now by use of LEU (<20%  $^{235}\text{U}$ )

$$\rightarrow N_{^{99}\text{Mo}} = \frac{\varphi \sigma_{^{235}\text{U}_f} \gamma_{^{99}\text{Mo}} N_{^{235}\text{U}_0}}{\lambda_{^{99}\text{Mo}}} [1 - e^{-\lambda_{^{99}\text{Mo}} t}] \quad (\gamma = \text{fission production probability})$$

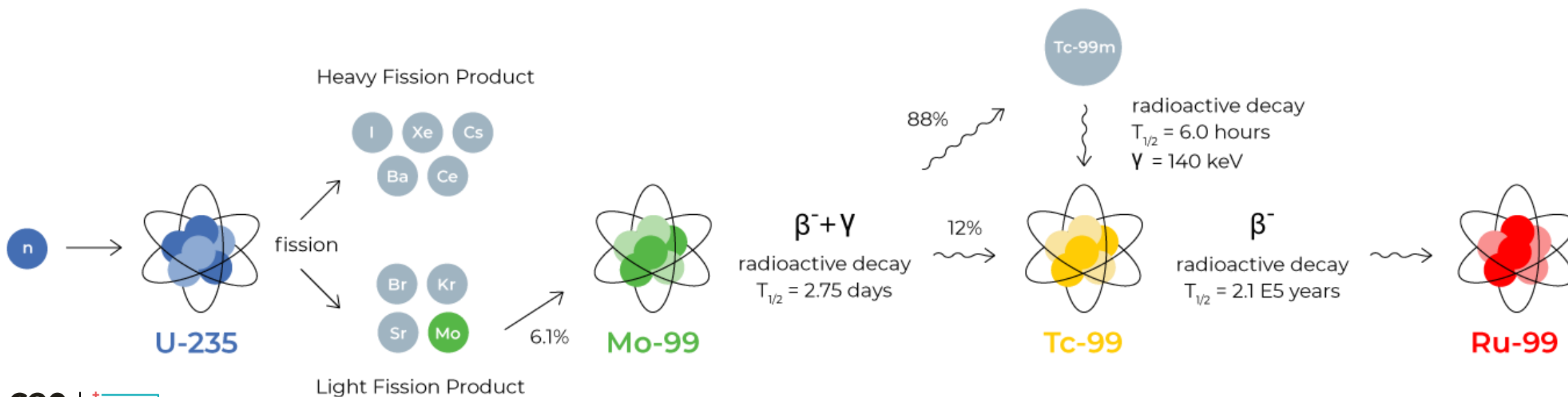


Reference Target	HEU (93% $^{235}\text{U}$ )	LEU (19.8% $^{235}\text{U}$ )
$^{99}\text{Mo}$ yield, Ci	530	540
Total U ( $^{235}\text{U}$ ), g	16 (15)	94 (18)
$^{239}\text{Pu}$ , $\mu\text{Ci}$	30	720
$^{234}, ^{235}, ^{238}\text{U}$ , $\mu\text{Ci}$	1280	840
Total $\alpha$ , $\mu\text{Ci}$	1310	1560

Source: <https://www-nds.iaea.org/sgnucdat/c1.htm>

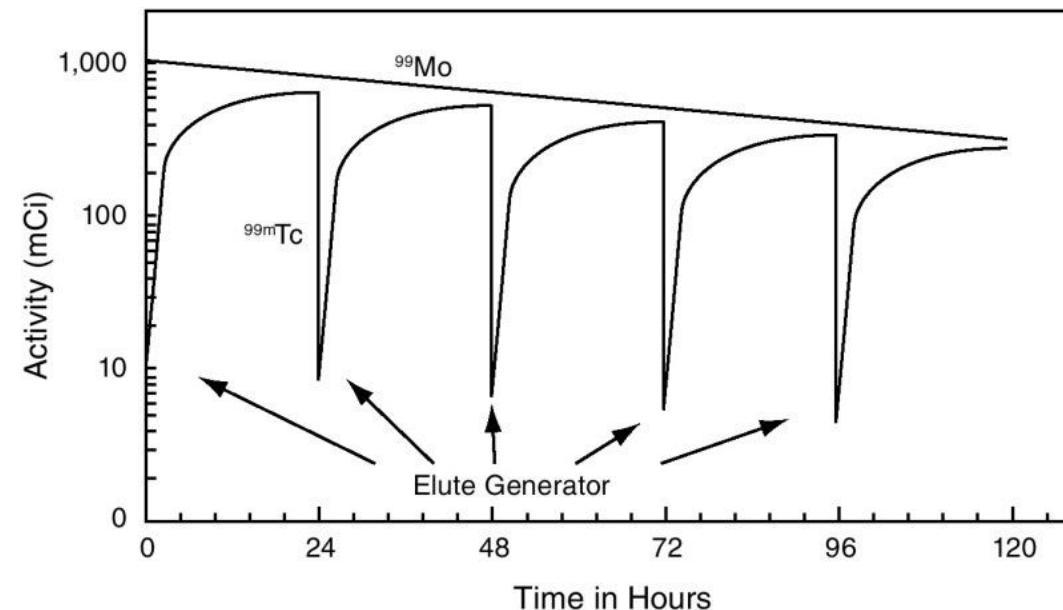
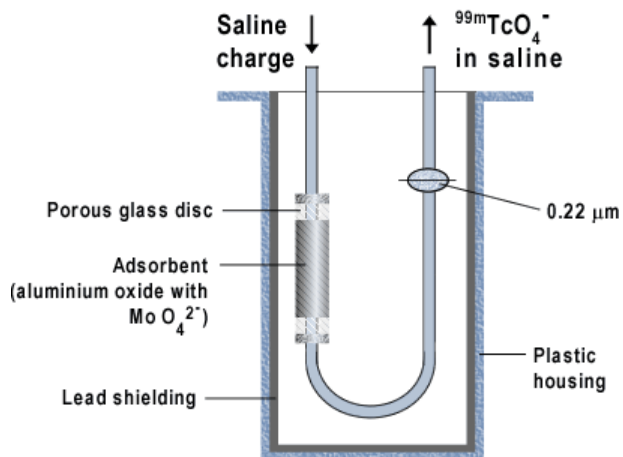
# Mo-99/Tc-99m production

- Used for diagnosis in hospitals (SPECT imaging)
- $^{99}\text{Mo}$  yield accounts for 5-7% of fission products
- $^{99}\text{Mo}/^{99\text{m}}\text{Tc}$  generators, locally milked for  $^{99\text{m}}\text{Tc}$
- Currently the working horse in nuclear medicine (80% ~ 40 million procedures)
- $^{99}\text{Mo}$  ( $t_{1/2} = 2.75 \text{ d}$ ),  $^{99\text{m}}\text{Tc}$  ( $t_{1/2} = 6 \text{ h}$ ) → Supply chain is race against time!



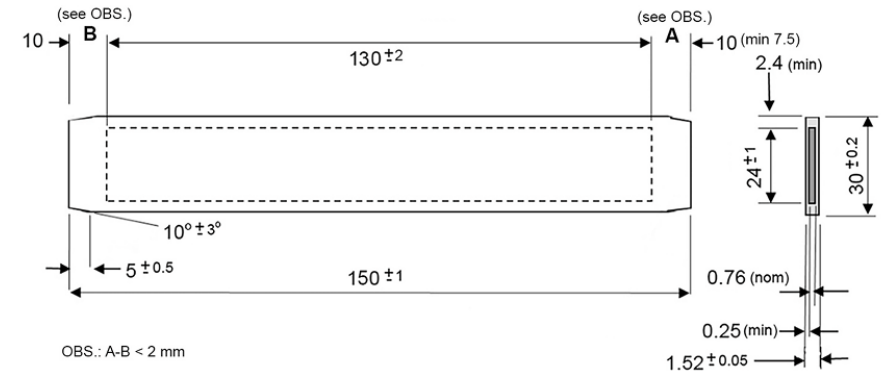
# Mo-99/Tc-99m production

- Used for diagnosis in hospitals (SPECT imaging)
- $^{99}\text{Mo}$  yield accounts for 5-7% of fission products
- $^{99}\text{Mo}/^{99\text{m}}\text{Tc}$  generators, locally milked for  $^{99\text{m}}\text{Tc}$
- Currently the working horse in nuclear medicine (80% ~ 40 million procedures)
- $^{99}\text{Mo}$  ( $t_{1/2} = 2.75 \text{ d}$ ),  $^{99\text{m}}\text{Tc}$  ( $t_{1/2} = 6 \text{ h}$ ) → Supply chain is race against time!



# Mo-99/Tc-99m production

1. Target manufacturing (LEU)
2. Production by  $^{235}\text{U}(\text{n},\text{f})$
3. Chemical extraction



## Target criteria

- **Properly sized** to fit into the irradiation position/canister
- Must contain a **sufficient amount of  $^{235}\text{U}$**  to produce required amount of  $^{99}\text{Mo}$
- **Good heat transfer properties** to prevent over-heating during irradiation
- **Provide a barrier** to the release of radioactive products during and after irradiation
- Target material must be **compatible with chemical processing steps** to recover and purify  $^{99}\text{Mo}$

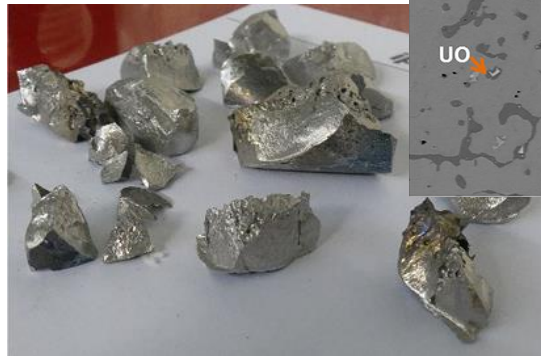


# Mo-99/Tc-99m production

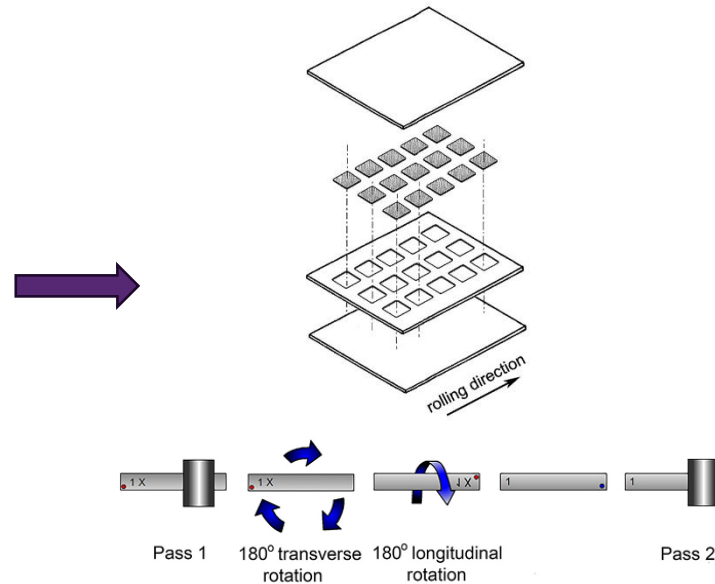
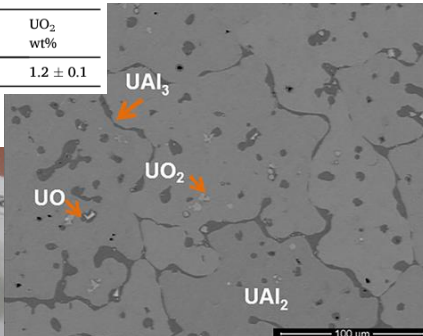
1. Target manufacturing (LEU)
2. Production by  $^{235}\text{U}(n,f)$
3. Chemical extraction

Phase composition in primary  $\text{UAl}_2$  ingot.

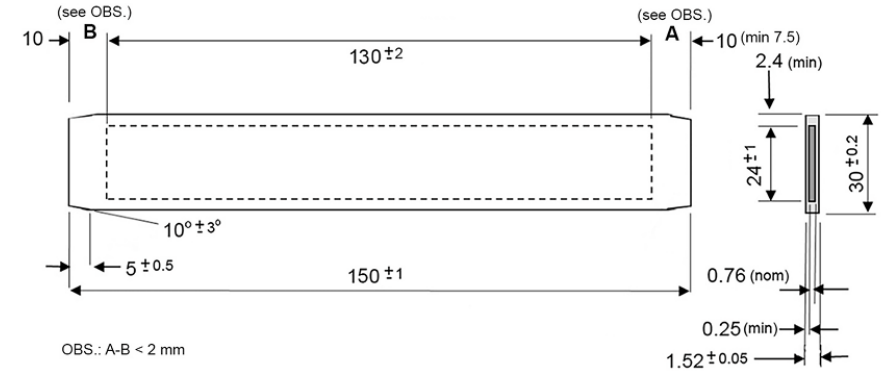
$\text{UAl}_2$ wt%	$\text{UAl}_3$ wt%	$\text{UAl}_4$ wt%	UO wt%	$\text{UO}_2$ wt%
$87.1 \pm 0.3$	$10.2 \pm 0.3$	N.D	$1.6 \pm 0.1$	$1.2 \pm 0.1$



$\text{UAl}_2$  ingots after induction melting  
(87 wt%  $\text{UAl}_2$ )



Hot-rolling to convert  $\text{UAl}_2$  into  $\text{UAl}_3$  and  $\text{UAl}_4$  according to picture-frame technique



Phase composition in the finished target.

$\text{UAl}_2$ wt%	$\text{UAl}_3$ wt%	$\text{UAl}_4$ wt%	UO wt%	$\text{UO}_2$ wt%
$0.3 \pm 0.1$	$30.1 \pm 1.5$	$68.1 \pm 1.6$	$0.3 \pm 0.1$	$1.3 \pm 0.2$

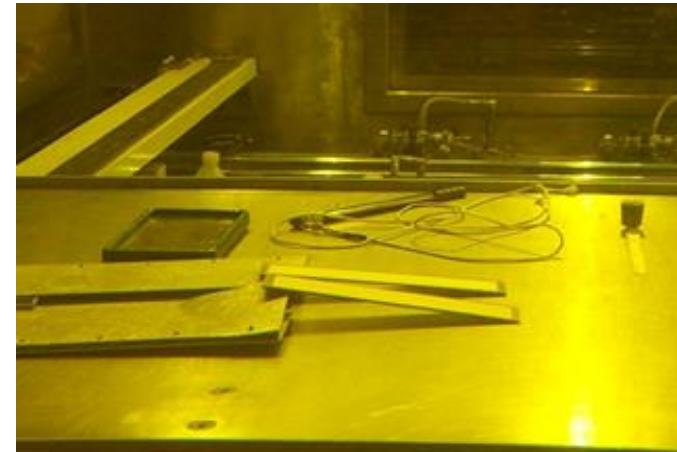
N.D = not detected.



$\text{UAl}_x$  meat completely surrounded by aluminium (cladding), guaranteeing removal of heat + isolation from reactor environment (0 wt%  $\text{UAl}_2$ )

# Mo-99/Tc-99m production

1. Target manufacturing (LEU)
2. Production by  $^{235}\text{U}(n,f)$
3. Chemical extraction

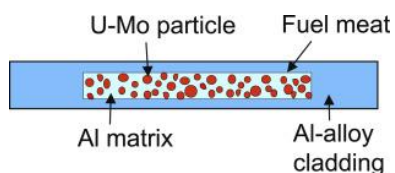


# Mo-99/Tc-99m production

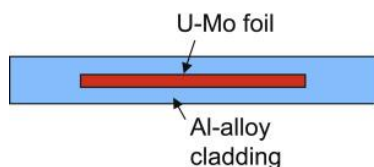


# Mo-99/Tc-99m production

1. Target manufacturing
2. Production by  $^{235}\text{U}(n,f)$
3. Chemical extraction



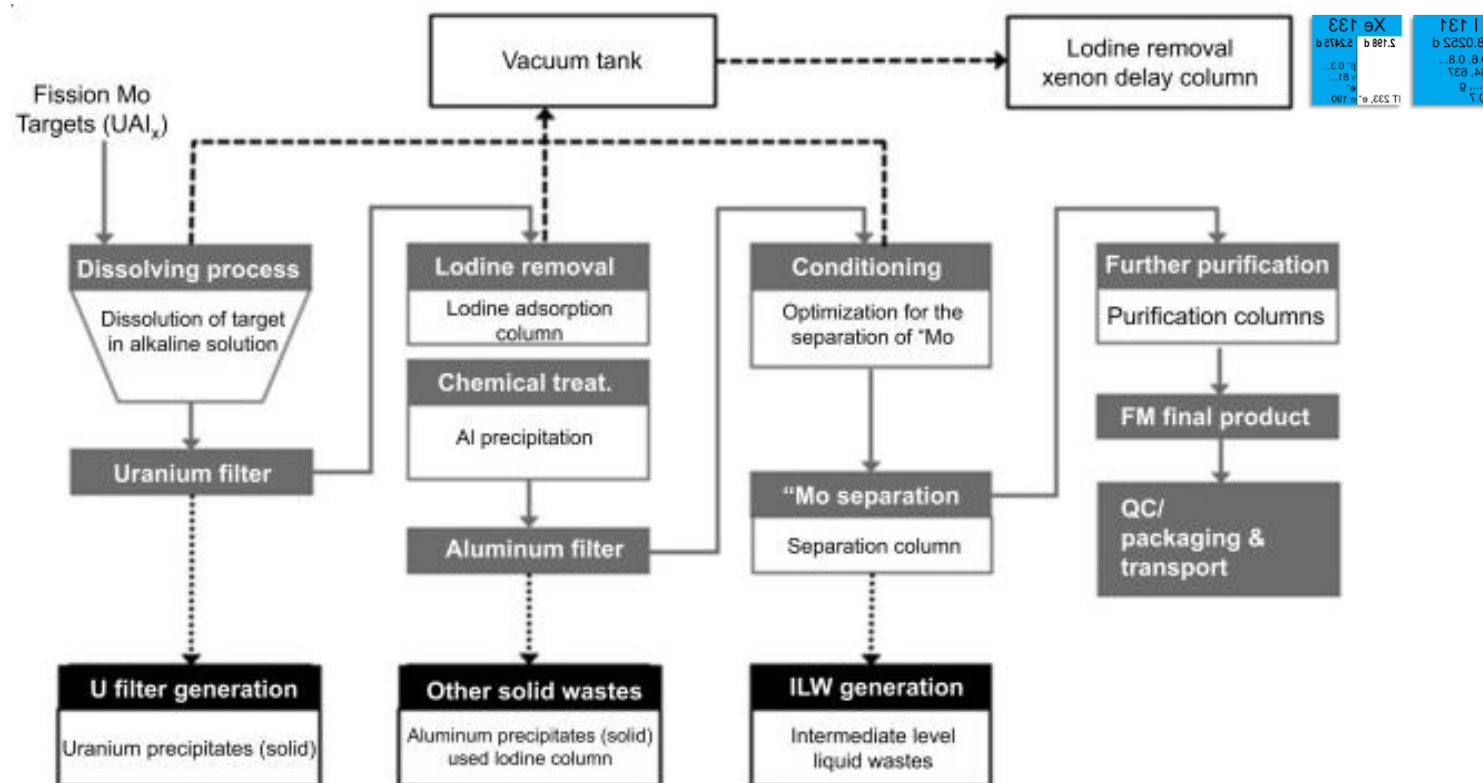
(a) Dispersion fuel



(b) Monolithic fuel

### Dissolution of target by NaOH

Yields a  $\text{NaAlO}_2 + \text{Na}_2\text{MoO}_4$  solution  
and solid oxide/hydroxide residu (U and most fission  
products)





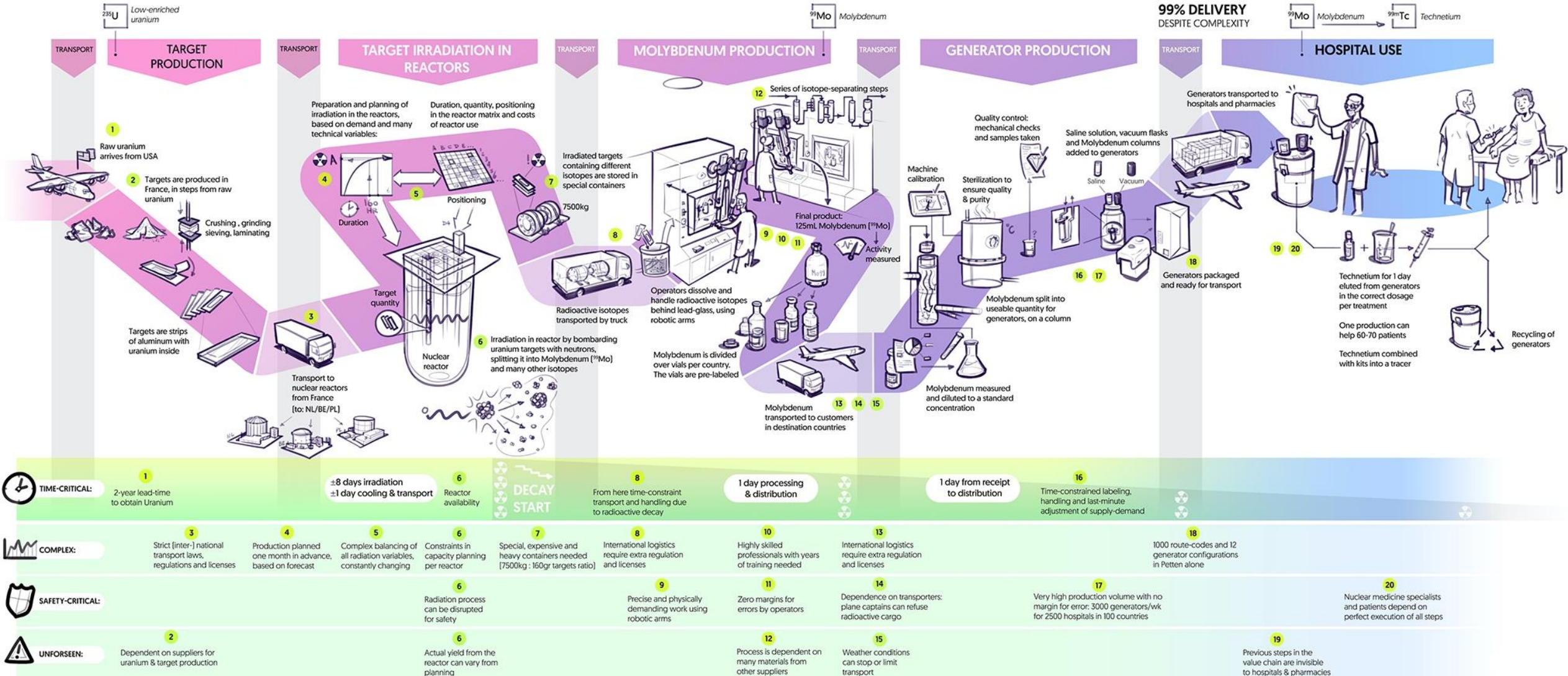
# Mo-99/Tc-99m production



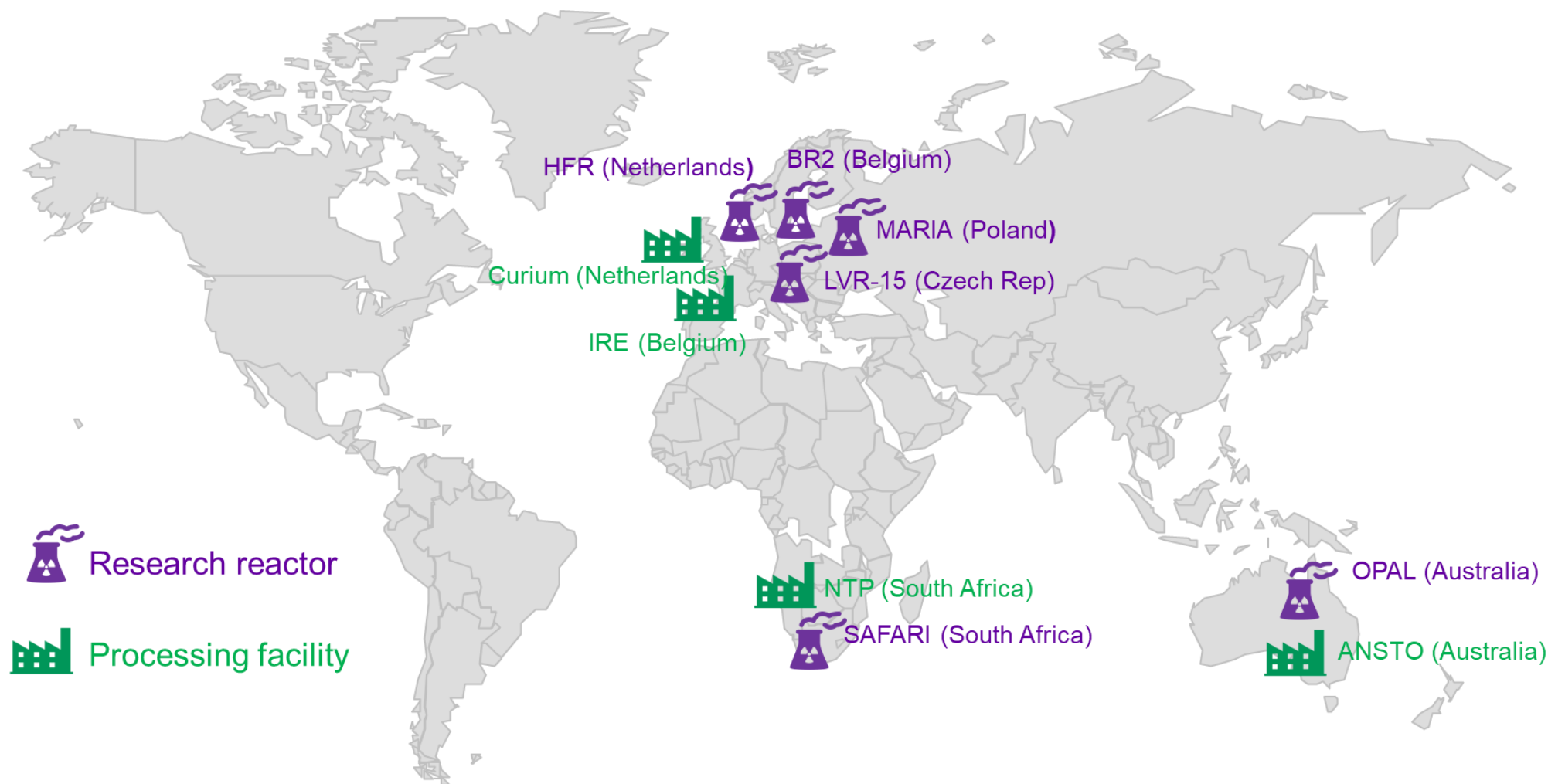


# COMPLEXITY OF GLOBAL MOLYBDENUM-99 SUPPLY CHAIN

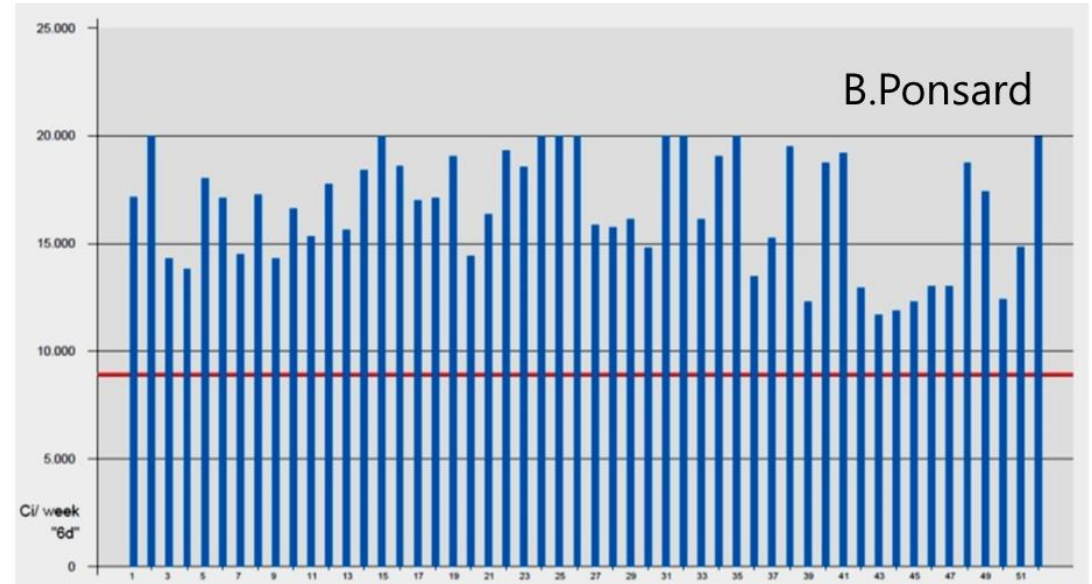
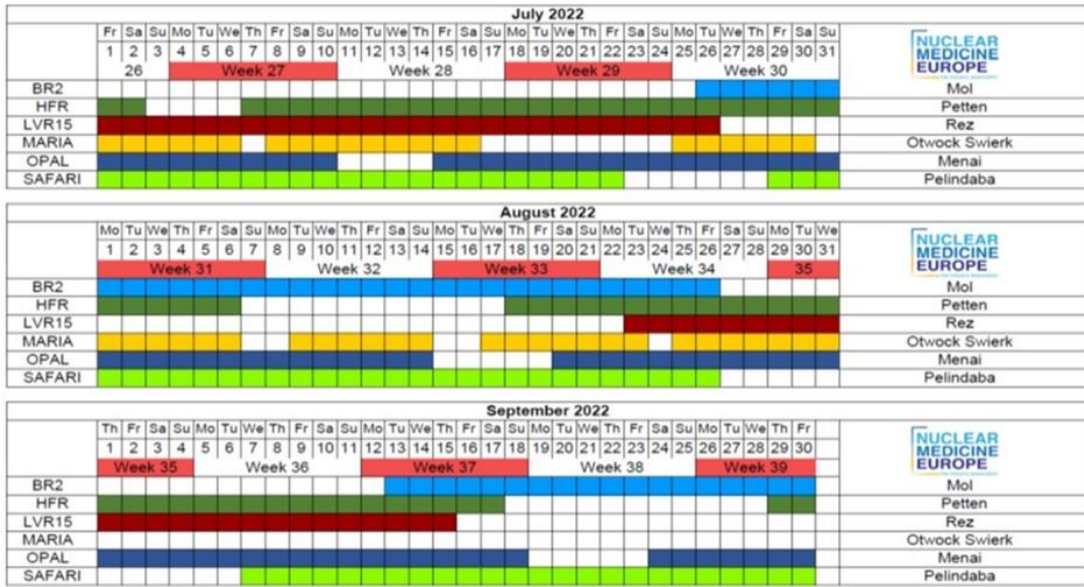
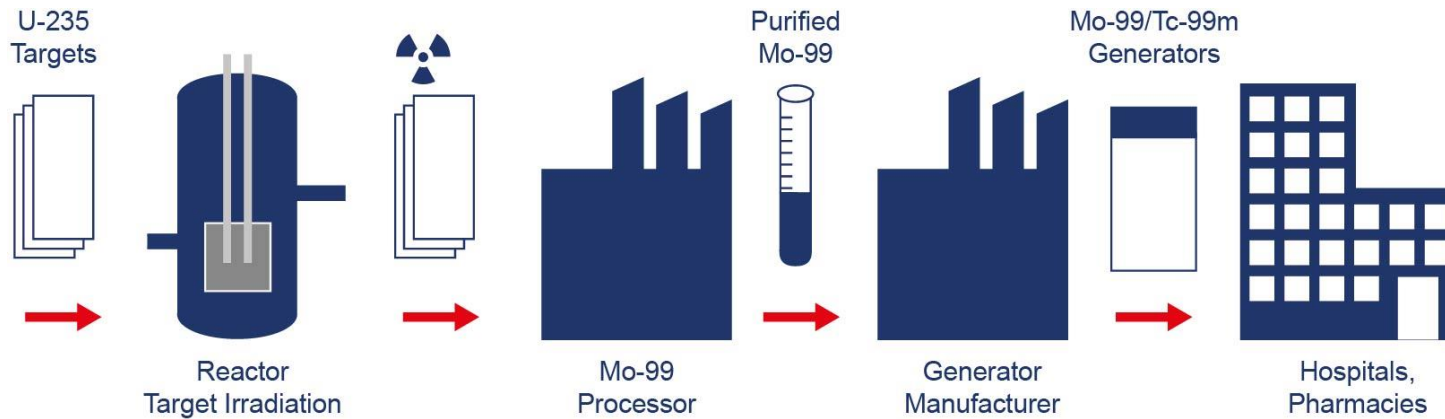
From target production to generator delivery



# Mo-99/Tc-99m production



# Mo-99/Tc-99m production – Security of supply





# Mo-99/Tc-99m production

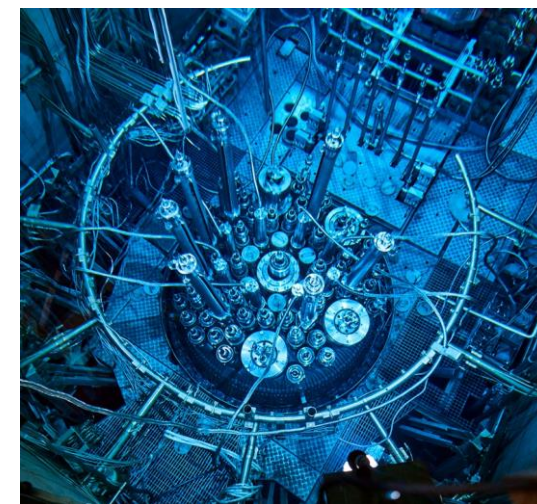
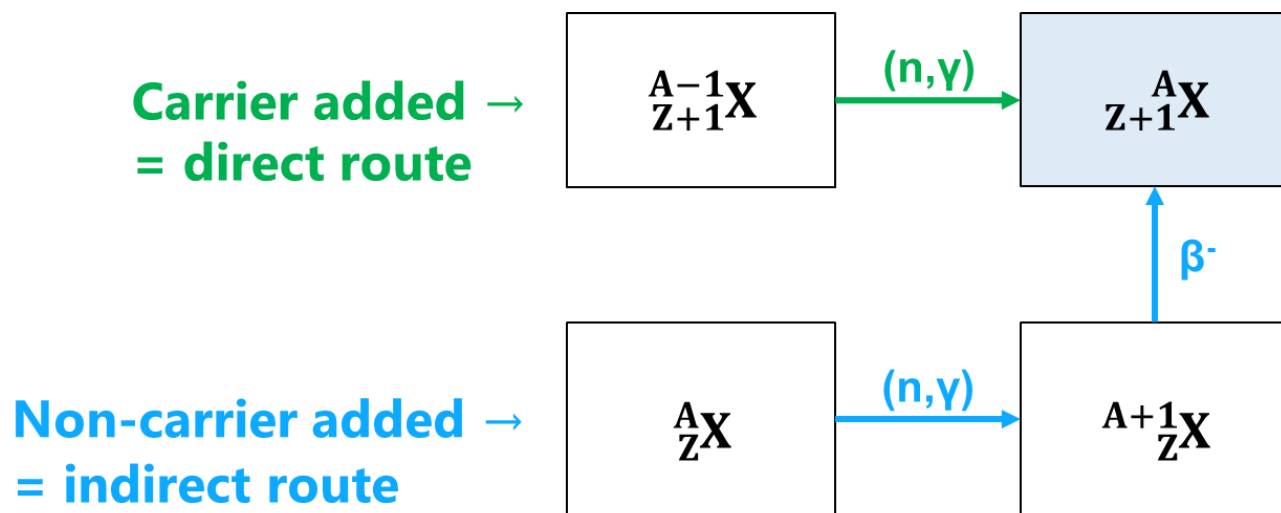
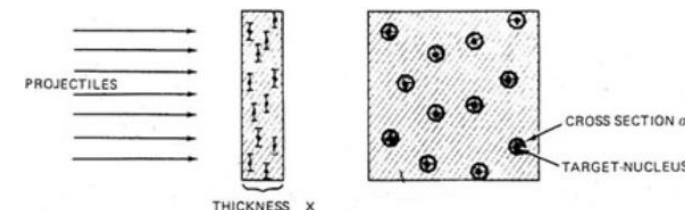
Reactor	Targets	Operating days/year	Mo-99 irradiation weeks/year	Irradiation capacity per week (6-day Ci Mo-99)	Irradiation capacity per year (6-day Ci Mo-99)	Estimated end of operation
BR2	LEU	203	29	8 600	249 400	2036
HFR	LEU	265	38	6 200	235 600	2030
LVR-15	LEU	210	30	3 000	90 000	2028
MARIA	LEU	200	36	2 200	79 200	2040
OPAL	LEU	308	44	3 200	140 800	2057
SAFARI-1	LEU	305	44	3 000	130 700	2030

Processor	Targets	Mo -99 production weeks/year	Processing capacity per week (6-day Ci Mo-99)	Processing capacity per year (6-d Ci Mo-99)	Estimated end of operation
ANSTO	LEU	44	3 200	140 800	2057
CURIUM	LEU	52	5 000	260 000	Not Known
IRE	LEU	52	3 500	182 000	At least until 2032
NTP	LEU	44	3 000	130 700	At least until 2030

# Production strategies – Neutron activation

Neutron activation  ${}^A\text{X}(n,\gamma){}^{A+1}\text{X}$

$$A = N_{\text{target}} \cdot \Delta_{\text{target}} \cdot \sigma_{\text{target}} \cdot \Phi_{\text{reactor}} \cdot (1 - e^{-\lambda_{\text{isotope}} \cdot t_{\text{irradiation}}})$$





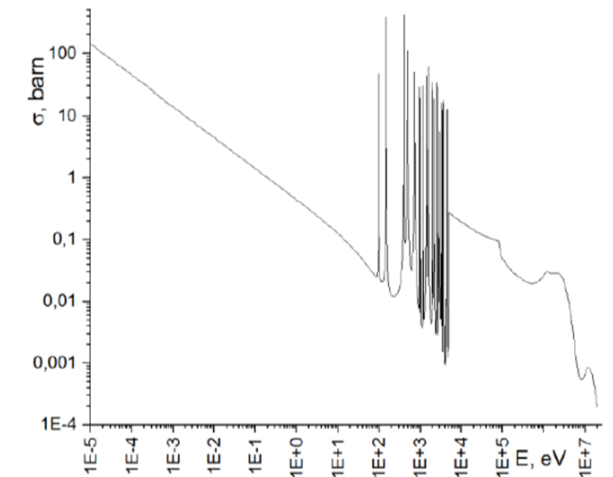
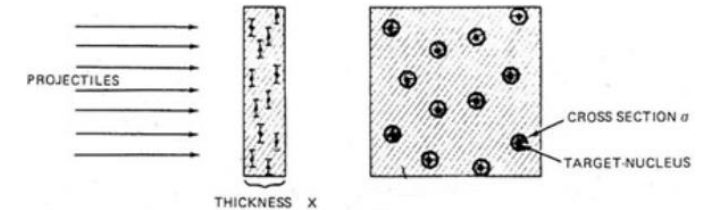
# Production strategies – Neutron activation

Neutron activation  $^A\text{X}(\text{n},\gamma)^{A+1}\text{X}$

$$A = N_{\text{target}} \cdot \Delta_{\text{target}} \cdot \sigma_{\text{target}} \cdot \phi_{\text{reactor}} \cdot (1 - e^{-\lambda_{\text{isotope}} \cdot t_{\text{irradiation}}})$$

Main factors that determine the production yield of the radionuclide of interest are:

- **Energy** of the neutrons and the **neutron flux**
- Characteristics of the **target material** (purity, enrichment, matrix, dimensions)
- **Activation cross-section** for the desired reaction



Cross-section of  $^{176}\text{Yb}$

Radionuclide	Half life	Application	Production method
$^{99}\text{Mo}/^{99\text{m}}\text{Tc}$	66 h/6 h	SPECT	$^{235}\text{U}$ fission $^{98}\text{Mo}(n,\gamma)^{99}\text{Mo}$
$^{131}\text{I}$	8 d		$^{235}\text{U}$ fission $^{130}\text{Te}(n,\gamma)^{131}\text{Te} \rightarrow ^{131}\text{I}$
$^{51}\text{Cr}$	28 d	Radionuclide therapy	$^{50}\text{Cr}(n,\gamma)^{51}\text{Cr}$
$^{153}\text{Sm}$	46 h		$^{152}\text{Sm}(n,\gamma)^{153}\text{Sm}$
$^{161}\text{Tb}$	6.95 d		$^{160}\text{Gd}(n,\gamma)^{161}\text{Gd} \rightarrow ^{161}\text{Tb}$
$^{166}\text{Ho}$	27 h		$^{165}\text{Ho}(n,\gamma)^{166}\text{Ho}$ $^{164}\text{Dy}(2n,\gamma)^{166}\text{Dy} \rightarrow ^{166}\text{Ho}$
$^{177}\text{Lu}$	6.65 d		$^{176}\text{Lu}(n,\gamma)^{177}\text{Lu}$ $^{176}\text{Yb}(n,\gamma)^{177}\text{Yb} \rightarrow ^{177}\text{Lu}$
$^{90}\text{Y}$	64 h		$^{89}\text{Y}(n,\gamma)^{90}\text{Y}$
$^{188}\text{W}/^{188}\text{Re}$	69.8 d/17 h		$^{186}\text{W}(2n,\gamma)^{188}\text{W} \rightarrow ^{188}\text{Re}$
$^{125}\text{I}$	60 d	Brachytherapy	$^{124}\text{Xe}(n,\gamma)^{125\text{m}}\text{Xe} \rightarrow ^{125}\text{I}$
$^{192}\text{Ir}$	74 d		$^{191}\text{Ir}(n,\gamma)^{192}\text{Ir}$

# Neutron activation – Examples

Hf 177	Hf 178	Hf 179
51.4 m IT 214 e <sup>-</sup> γ 277 295 327... m <sub>1</sub>	1.09 s 18.58 IT (13) e <sup>-</sup> γ 574 495... m <sub>1</sub>	31 a 4.0 s 27.28 IT 89... γ 426 326 m <sub>1</sub>
Lu 176	Lu 177	Lu 178
2.599 3.68 h β <sup>-</sup> 1.2 1.3... e <sup>-</sup> γ 88... e <sup>-</sup>	7 m 160.4 d β <sup>-</sup> 0.2 γ 208 m <sub>1</sub> IT 1003 γ 1003 IT (146) e <sup>-</sup> γ 414... m <sub>1</sub>	22.7 m 28.4 m β <sup>-</sup> 2.0... γ 93, 1341 1310 1269... g
Yb 175	Yb 176	Yb 177
4.185 d β <sup>-</sup> 0.5... γ 396, 283 114...	11.4 s 12.887 IT 96 σ 2.85 γ 293, 389 σ <sub>n,α</sub> 190, 82, e <sup>-</sup> σ < 1E-6	6.41 s 1.911 h β <sup>-</sup> 1.4... γ 150 1080 1242 122... e <sup>-</sup> γ 105

Er 166	Er 167	Er 168
33.503 σ 15.0 + 1.9 σ <sub>n,α</sub> < 7E-5	2.269 s IT 208 e <sup>-</sup> σ 649 σ <sub>n,α</sub> < 7E-5	22.869 26.978 σ 2.74, σ <sub>n,α</sub> 9E-5
Ho 165	Ho 166	Ho 167
100 σ 3.5 + 60.9 σ <sub>n,α</sub> < 2E-5	1132.6 a β <sup>-</sup> 1.8 γ 184, 810 12... 10778 e <sup>-</sup>	26.824 h 3.1 h β <sup>-</sup> 0.3, 1.0... γ 347, 321... m <sub>1</sub>
Dy 164	Dy 165	Dy 166
28.260 σ 1610 + 1040	1.257 m IT 108, e <sup>-</sup> γ 150 1.0... γ 515... σ 2000	2.334 h 81.5 h β <sup>-</sup> 1.3... (362...) γ 95 82, (426...) g

Dy 161	Dy 162	Dy 163
18.889 σ 600, σ <sub>n,α</sub> < 3E-5	25.475 σ 194	24.896 σ 134, σ <sub>n,α</sub> < 2E-5
Tb 160	Tb 161	Tb 162
72.3 d β <sup>-</sup> 0.6, 1.7... γ 879, 299 966... σ 570	6.89 d β <sup>-</sup> 0.5, 0.6... γ 26, 49, 75... e <sup>-</sup>	7.76 m β <sup>-</sup> 1.4, 2.4... γ 260, 808 388...
Gd 159	Gd 160	Gd 161
18.479 h β <sup>-</sup> 1.0... γ 364, 58...	21.86 σ 1.4	3.66 m β <sup>-</sup> 1.6, 1.7... γ 361, 315 102... σ 19000

Os 188	Os 189	Os 190
13.24 σ 5.5, σ <sub>n,α</sub> < 3E-5	5.81 h 16.15 σ 0.00026 + 25 σ < 1E-5	9.9 m 26.26 IT (39) e <sup>-</sup> γ 616 503, 361 σ <sub>n,α</sub> < 2E-5
Re 187	Re 188	Re 189
62.60 4.33·10 <sup>10</sup> a β <sup>-</sup> 0.0026 no γ σ 2.05 + 72.75	18.59 m 17.005 h IT (2, 16) e <sup>-</sup> γ 155 633... σ < 2	24.3 h β <sup>-</sup> 1.0... γ 217, 219, 245 86, 147... e <sup>-</sup> m <sub>1</sub>
W 186	W 187	W 188
28.43 σ 38.1	23.72 h β <sup>-</sup> 0.6, 1.3... γ 686, 480, 72... σ 64	69.78 d β <sup>-</sup> 0.3... γ (291, 227...) g

Xe 131	Xe 132	Xe 133
11.86 d IT 164, e <sup>-</sup> σ 93	21.232 26.909 σ 0.05 + 0.40	2.198 d 5.2475 d β <sup>-</sup> 0.3... γ 81... e <sup>-</sup> σ 190
I 130	I 131	I 132
8.84 m β <sup>-</sup> 1.0 1.8... IT (40), e <sup>-</sup> γ 536, 66 β <sup>-</sup> 2.5... 739 γ 536... σ 18	12.36 h 8.0252 d β <sup>-</sup> 0.6, 0.8... γ 364, 637 284... g σ -0.7	1.387 h 2.295 h IT 98, e <sup>-</sup> 227 γ 1.5... β <sup>-</sup> 2.1... 668, 773 00, 175... 955, 523...
Te 129	Te 130	Te 131
33.6 d IT (106) e <sup>-</sup> β <sup>-</sup> 1.6... γ 696...	69.6 m 34.08 6.8·10 <sup>20</sup> a β <sup>-</sup> 1.5... γ 28, 460 487... e <sup>-</sup> σ 0.010 + 0.185	33.25 h 25.0 m β <sup>-</sup> 2.1... γ 774 852... IT (182), e <sup>-</sup> 452...

Eu 153	Eu 154
52.19 σ 312, σ <sub>n,α</sub> 1E-5	46.0 m 8.601 a β <sup>-</sup> 0.6, 1.8... γ 123, 1274 723, 1005... e <sup>-</sup> γ 68 101 e <sup>-</sup> γ 1446
Sm 152	Sm 153
26.74 σ 206	46.284 h β <sup>-</sup> 0.7, 0.8... γ 103, 70... e <sup>-</sup> σ 420

Ru 99	Ru 100	Ru 101
12.76 σ 7.25	12.60 5.8	17.06 σ 5.2
Tc 98	Tc 99	Tc 100
4.2·10 <sup>6</sup> a β <sup>-</sup> 0.4 γ 745, 652 σ 0.93 + ?	6.0072 h 2.111·10 <sup>5</sup> s IT (143, 2) e <sup>-</sup> γ 141 β <sup>-</sup> ... γ (90...) σ 22.8	15.65 s β <sup>-</sup> 3.2... γ 540, 591...
Mo 97	Mo 98	Mo 99
9.582 σ 2.2, σ <sub>n,α</sub> 4E-7	24.292 σ 0.130	65.924 h β <sup>-</sup> 2... γ 740, 181 778... m, g

# Production strategies – $^{177}\text{Lu}$ example

$^{176}\text{Lu}(n,\gamma)^{177}\text{Lu}$  ( $\sigma_{\text{th}} = 2057$  barn) but  $^{176}\text{Lu}(n,\gamma)^{177\text{m}}\text{Lu}$  ( $\sigma_{\text{th}} = 2.8$  barn)



$\updownarrow$   
 $^{176}\text{Yb}(n,\gamma)^{177}\text{Lu}$  ( $\sigma_{\text{th}} = 2.85$  barn)

endolucin  
beta



Tradeoff between

- Production yield
  - Specific activity
  - Chemical and radionuclidic purity
- Depends on available target material and final application

Hf 177			Hf 178			Hf 179		
51.4 m	1.09 s	18.58	31 a	4.0 s	27.28	25.05 d	18.67 s	13.63
IT 214			IT (13)			IT 257		
e <sup>-</sup>			e <sup>-</sup>			(21), e <sup>-</sup>	IT	
γ 277	IT 228...		γ 574	IT 89...		γ 454	161...	
295	e <sup>-</sup>	σ 2E-7	495...	γ 426		363...	e <sup>-</sup>	σ 0.445
327...	γ 208	+ 0.96	m <sub>1</sub>	326	σ ? + 53		γ 214	+ 41
m <sub>1</sub>	379...	+ 374	γ 45	213	+ 30			
Lu 176			Lu 177			Lu 178		
2.599			7 m	160.4 d	6.6443 d	22.7 m	28.4 m	
3.68 h	3.8·10 <sup>10</sup> a		β 0.2	β <sup>-</sup>		β <sup>-</sup> 2.0...		
β <sup>-</sup> 1.2	β <sup>-</sup> 0.6...		γ 208	0.5...		γ 93, 1341		
1.3...	γ 307, 202		β <sup>-</sup> 228...	γ 208		γ 1.2...	1310	
e <sup>-</sup>	88...		IT 1003	IT (146), e <sup>-</sup>	113...	332...	1269...	
γ 88...	σ 2.8+205		m <sub>2</sub>	γ 414...	σ 880			
Yb 175			Yb 176			Yb 177		
4.185 d			11.4 s	12.887		6.41 s	1.911 h	
β <sup>-</sup> 0.5...			IT 96	σ 2.85		β <sup>-</sup> 1.4...		
γ 396, 283			γ 293, 389	σ <sub>n,α</sub>		γ 150		
114...			190, 82, e <sup>-</sup>	<1E-6		1080		
						1242		
						122...	e <sup>-</sup>	
						γ 105		

# Production strategies – $^{177}\text{Lu}$ example

$^{176}\text{Lu}(n,\gamma)^{177}\text{Lu}$  ( $\sigma_{\text{th}} = 2057 \text{ barn}$ ) but  $^{176}\text{Lu}(n,\gamma)^{177\text{m}}\text{Lu}$  ( $\sigma_{\text{th}} = 2.8 \text{ barn}$ )

$A(^{177}\text{Lu}) = 1115 \text{ TBq at EOI}$

→  $SA(^{177}\text{Lu}) = 1115 \text{ GBq/mg}$

$A(^{177}\text{Lu}) = 527 \text{ TBq at EOI+7d}$

→  $SA(^{177}\text{Lu}) = 527 \text{ GBq/mg}$

$^{176}\text{Yb}(n,\gamma)^{177}\text{Lu}$  ( $\sigma_{\text{th}} = 2.85 \text{ barn}$ )

$A(^{177}\text{Lu}) = 1.5 \text{ TBq at EOI}$

→  $SA(^{177}\text{Lu}) = 4106 \text{ GBq/mg}$

$A(^{177}\text{Lu}) = 0.8 \text{ TBq at EOI+7d}$

→  $SA(^{177}\text{Lu}) = 4106 \text{ GBq/mg}$



Hf 177	Hf 178	Hf 179
51.4 m IT 214 e <sup>-</sup> γ 277 295 327... m <sub>1</sub>	1.09 s 18.58 IT 228... e <sup>-</sup> γ 208 379... m <sub>1</sub>	31 a 4.0 s 27.28 IT (13) e <sup>-</sup> γ 574 495... m <sub>1</sub>
25.05 d 18.67 s 13.63 IT 257 (21), e <sup>-</sup> IT 161... e <sup>-</sup> γ 214 + 41	25.05 d 18.67 s 13.63 IT 257 (21), e <sup>-</sup> IT 161... e <sup>-</sup> γ 214 + 41	25.05 d 18.67 s 13.63 IT 257 (21), e <sup>-</sup> IT 161... e <sup>-</sup> γ 214 + 41
Lu 176	Lu 177	Lu 178
3.68 h β <sup>-</sup> 1.2 1.3... e <sup>-</sup> γ 88... e <sup>-</sup>	7 m 160.4 d 6.643 d β <sup>-</sup> 0.2 β <sup>-</sup> γ 208 228... m <sub>1</sub> IT (116), e <sup>-</sup> 1003 IT (116), e <sup>-</sup> 88... m <sub>1</sub>	22.7 m 28.4 m β <sup>-</sup> 2.0... γ 93, 1341 1310 1269... g
Yb 175	Yb 176	Yb 177
4.185 d β <sup>-</sup> 0.5... γ 396, 283 114...	11.4 s 12.887 IT 96 γ 293, 389 190, 82, e <sup>-</sup>	6.41 s 1.911 h β <sup>-</sup> 1.4... γ 150 1080 1242 122... e <sup>-</sup> γ 105

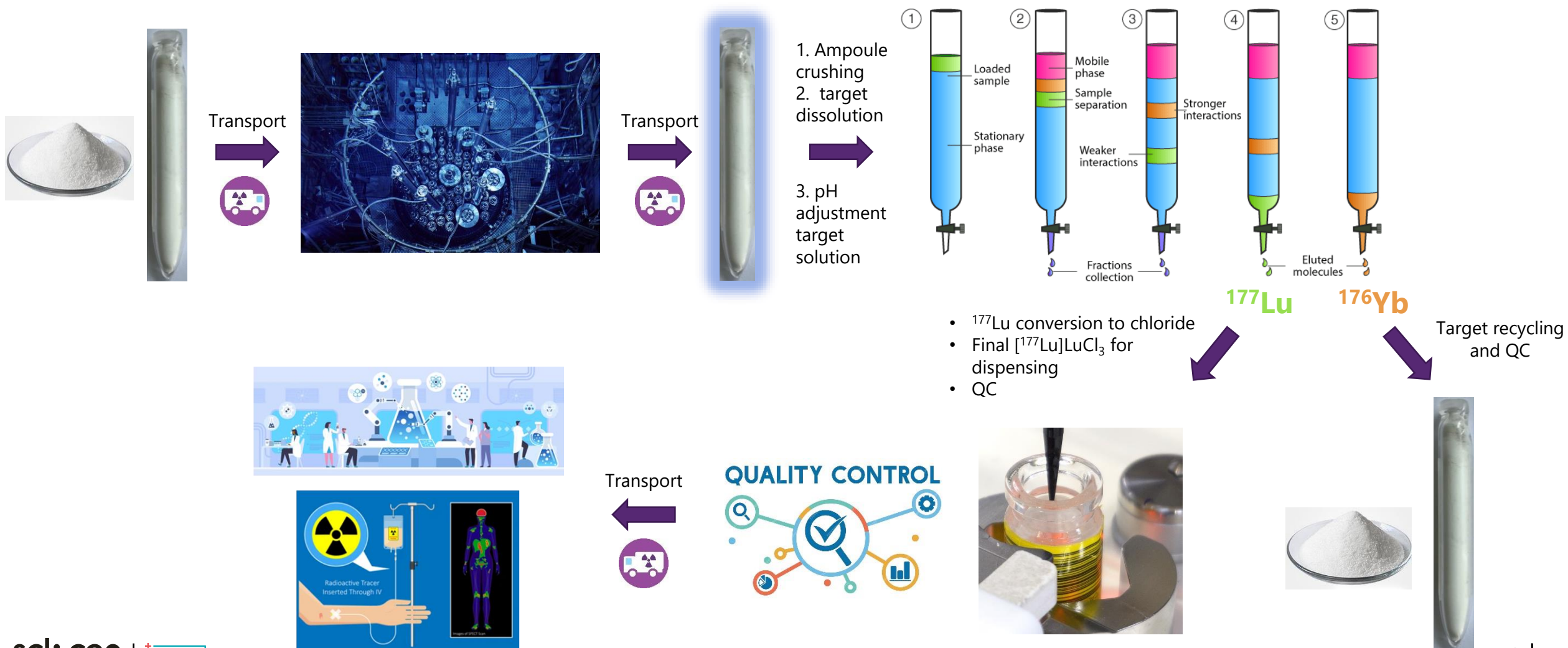
## Activation parameters

- 100% enriched target
- $\Phi_{\text{th}} = 3\text{E}14 \text{ neutrons/cm}^2/\text{s}$
- No epithermal or fast neutrons
- No self-shielding
- 7 days irradiation
- 1 g target

$$A = N_{\text{target}} \cdot \sigma_{\text{th, target}} \cdot \Phi_{\text{th, reactor}} \cdot (1 - e^{-\lambda_{\text{isotope}} \cdot t_{\text{irr}}}) \cdot e^{-\lambda_{\text{isotope}} \cdot t_{\text{cool}}}$$



# Production n.c.a. $^{177}\text{Lu}$ – General approach





# Target

---

Target manufacturing  
and irradiation

Radiochemical  
processing

Quality control

Target recovery and  
recycling

Waste management

## Target preparation

### Target criteria

- **Properly sized** to fit into the irradiation position/canister
- Sufficient amount to produce desired amount of activity
- **Good heat transfer properties** to prevent over-heating during irradiation
- **Thermally stable compounds** to prevent pressure build-up and target failure → typically metal or oxide compounds
- **Provide a barrier** to the release of radioactive products during and after irradiation
- Target material must be **compatible with chemical processing steps** to recover and purify desired radioactive compound

# Target

Target manufacturing  
and irradiation

Radiochemical  
processing

Quality control

Target recovery and  
recycling

Waste management

## Target preparation

Target matrix should be suitable for neutron activation

→ **Radiolanthanides**: typically  $\text{Ln}_2\text{O}_3$  target material sealed in a quartz glass ampoule (1 mm wall thickness) in cold welded aluminium irradiation can

$\text{Ln}(\text{NO}_3) \cdot x\text{H}_2\text{O}$		$\text{Ln}_2\text{O}_3$	
More time-consuming target preparation	☹️	Simple target preparation	😊
Easy to dissolve for chemical separation	😊	More challenging to dissolve	😐
Hygroscopic nature	☹️	Not hygroscopic	😊
Low thermal stability, increased risk of ampoule failure	☹️	High thermal stability, enhancing target stability	😊
Lower density = lower loading capacity	☹️	Higher density = higher loading capacity	😊

# Target

Target manufacturing  
and irradiation

Radiochemical  
processing

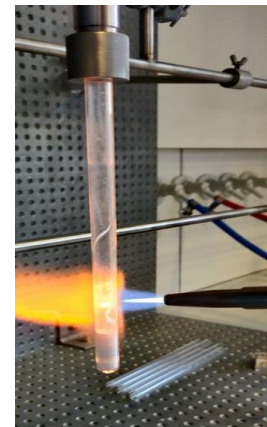
Quality control

Target recovery and  
recycling

Waste management

## Target preparation

- Target matrix should be suitable for neutron activation
  - **Radiolanthanides**: typically  $\text{Ln}_2\text{O}_3$  target material sealed in a quartz glass ampoule (1 mm wall thickness) in cold welded aluminium irradiation can
  - Metal compounds (e.g.  $^{186}\text{W}$  rings,  $^{176}\text{Yb}$  in SHINE process)
- Ampoule size limited to dimensions of aluminium irradiation can
  - Relatively uniform, but small variations between different research reactors





# $^{177}\text{Lu}$ production – Target quality

Hf 170 16.01 h $\epsilon$ $\gamma$ 165, 621, 120 573...	Hf 171 29.5 s 12.1 h $\epsilon$ , $\beta^+$ ? $\gamma$ 662 122 1071... IT (22) $e^-$ $\epsilon$ ? g, m	Hf 172 1.87 a $\epsilon$ $\gamma$ 24, 126, 67 82... m	Hf 173 23.6 h $\epsilon$ $\gamma$ 124, 297, 140 311...	Hf 174 0.161 $2.0 \cdot 10^{15}$ a $\alpha$ 2.500 $\sigma$ 549	Hf 175 70.0 d $\epsilon$ $\gamma$ 343...	Hf 176 5.24 $\sigma$ 23.5	Hf 177 51.4 m 1.09 s 18.58 IT 214 $e^-$ $\gamma$ 277 295 327... IT 228... $e^-$ $\gamma$ 208 379 $\sigma$ 2E-7 + 0.1 m1 374 46 213... + 30 g	Hf 178 31 a 4.0 s 27.28 IT (13) $e^-$ ... $\gamma$ 574 495... $\gamma$ 426 326 $\sigma$ ? + 53 363... + 30 g	Hf 179 25.05 d 18.67 s 13.63 IT 257 (21), $e^-$ IT $\gamma$ 454 161... $e^-$ $\gamma$ 214 + 41 $\sigma$ 0.445
Lu 169 160 s 34.06 h $\epsilon$ $\beta^+$ ... $\gamma$ 961, 191 1450... IT (29) $e^-$ g, m	Lu 170 2.012 d $\epsilon$ $\beta^+$ ... $\gamma$ 84, 1280, 2042 985...	Lu 171 79 s 8.247 d $\epsilon$ $\beta^+$ ... $\gamma$ 740, 19 667, 76 781... IT (71) $e^-$	Lu 172 3.7 m 6.70 d $\epsilon$ $\gamma$ 1094 901, 181 810 912... IT (42) $e^-$	Lu 173 1.37 a $\epsilon$ $\gamma$ 272, 79, 101... $e^-$ $\sigma$ 34.3	Lu 174 142 d 3.31 a IT (59...), $e^-$ $\gamma$ 45, 67... $e^-$ $\epsilon$ $\beta^+$ ... $\gamma$ 1242 76...	Lu 175 97.401 $\sigma$ 16.7 + 6.6 $\sigma_{n,\alpha} < 6E-5$	Lu 176 2.599 3.68 h 3.8 $\cdot 10^{10}$ a $\beta^-$ 1.2 1.3... $\gamma$ 307, 202 88... $\sigma$ 2.8+2057 m2 $\sigma$ 417	Lu 177 7 m 160.4 d 6.6443 d $\beta^-$ 0.2 $\beta^-$ 0.5... $\gamma$ 208 228... m1 1003 IT (116), $e^-$ 113... $\gamma$ 332... $\sigma$ 880	Lu 178 22.7 m 28.4 m $\beta^-$ 2.0... $\gamma$ 93, 1341 1310 1269... g
Yb 168 0.126 $\sigma$ 3033 $\sigma_{n,\alpha} < 0.0001$	Yb 169 46 s 32.018 d $\epsilon$ $\gamma$ 63 198, 177 110... IT (24) $e^-$ $\sigma$ 3600	Yb 170 3.023 10.2 $\beta^-$ 1.0E-5	Yb 171 14.216 $\sigma$ 58.8 $\sigma$ 1.5E-6	Yb 172 21.754 $\sigma$ 1.3, $\sigma_{n,\alpha} < 1E-6$	Yb 173 16.098 $\sigma$ 15.5, $\sigma_{n,\alpha} < 1E-6$	Yb 174 31.896 $\sigma$ 63, $\sigma_{n,\alpha} < 2E-5$	Yb 175 4.185 d $\beta^-$ 0.5... $\gamma$ 396, 283 114...	Yb 176 11.4 s 12.887 6.41 s 1.911 h $\beta^-$ 1.4... $\gamma$ 150 1080 1242 122... $e^-$ g	Yb 177 11.4 s 12.887 6.41 s 1.911 h $\beta^-$ 1.4... $\gamma$ 150 1080 1242 122... $e^-$ g
Tm 167 9.25 d $\epsilon$ $\gamma$ 57, 532..., $e^-$ m	Tm 168 93.1 d $\epsilon$ , $\beta^+$ ... $\gamma$ 198, 816 448..., $e^-$ $\beta^-$ ...	Tm 169 100 $\sigma$ 107	Tm 170 128.6 d $\beta^-$ 1.0... $\gamma$ 84, $e^-$ $\epsilon$ , $\gamma$ (79) $\sigma$ 92	Tm 171 1.92 a $\beta^-$ 0.1... $\gamma$ (67), $e^-$ $\sigma$ ~160	Tm 172 63.6 h $\beta^-$ 1.8, 1.9... $\gamma$ 79, 1094 1387, 1530 1466, 1609...	Tm 173 8.24 h $\beta^-$ 0.9, 1.3... $\gamma$ 399, 461...	Tm 174 2.29 s 5.4 m IT 152, $e^-$ $\gamma$ 100, $e^-$ 273, 177...	Tm 175 15.2 m $\beta^-$ 0.9, 1.9... $\gamma$ 515, 941 364...	Tm 176 1.9 m $\beta^-$ 2.0, 2.8... $\gamma$ 190, 1069 382... g

Might affect target recycling

High affect specific activity  $^{177}\text{Lu}$



# $^{161}\text{Tb}$ production – Target quality

153 4 h	Dy 154 3.0·10 <sup>6</sup> a	Dy 155 9.9 h	Dy 156 0.056	Dy 157 8.14 h	Dy 158 0.095	Dy 159 144.4 d	Dy 160 2.329	Dy 161 18.889	Dy 162 25.475	Dy 163 24.896	Dy 164 1.14 a
152 17.5 h	Tb 153 2.34 d	Tb 154 22.7 h	Tb 155 5.32 d	Tb 156 5.3 h	Tb 157 71 a	Tb 158 10.70 s	Tb 159 100	Tb 160 72.3 d	Tb 161 6.89 d	Tb 162 7.76 m	Tb 163 1.14 a
151 20 d	Gd 152 0.20	Gd 153 240.4 d	Gd 154 2.18	Gd 155 14.80	Gd 156 20.47	Gd 157 15.65	Gd 158 24.84	Gd 159 18.479 h	Gd 160 21.86	Gd 161 3.66 m	Gd 162 1.14 a
150 36.9 a	Eu 151 47.81	Eu 152 96 m	Eu 153 52.19	Eu 154 46.0 m	Eu 155 4.753 a	Eu 156 15.19 d	Eu 157 15.18 h	Eu 158 45.9 m	Eu 159 18.1 m	Eu 160 30.8 s	Eu 161 42.6 s
149 8.82	Sm 150 7.37	Sm 151 94.7 a	Sm 152 26.74	Sm 153 46.284 h	Sm 154 22.74	Sm 155 22.18 m	Sm 156 9.4 h	Sm 157 8.03 m	Sm 158 5.30 m	Sm 159 11.37 s	Sm 160 1.14 a

Might create long-lived waste

# $^{161}\text{Tb}$ production – Target quality

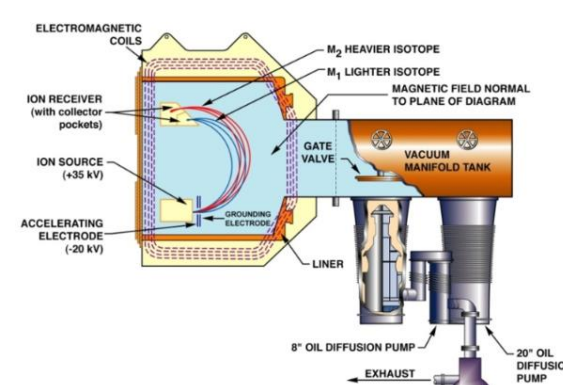
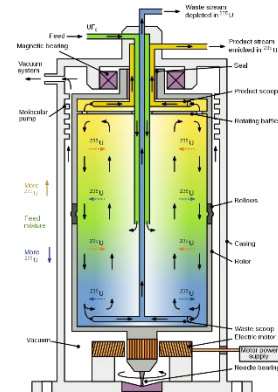
153 4 h	Dy 154 3.0·10 <sup>6</sup> a $\alpha$ 2.87	Dy 155 9.9 h $\beta^+$ 0.9, 1.1... $\gamma$ 227...	Dy 156 0.056 $\sigma$ 33 $\sigma_{n,\alpha} < 0.009$	Dy 157 8.14 h $\alpha, \beta^+$ ... $\gamma$ 326...	Dy 158 0.095 $\sigma$ 43 $\sigma_{n,\alpha} < 0.006$	Dy 159 144.4 d $\alpha$ $\gamma$ 58, e <sup>-</sup>	Dy 160 2.329 $\sigma$ 55	Dy 161 18.889 $\sigma$ 600, $\sigma_{n,\alpha} < 3\text{E-}5$	Dy 162 25.475 $\sigma$ 194	Dy 163 24.896 $\sigma$ 134, $\sigma_{n,\alpha} < 2\text{E-}5$	Dy 164 24.896 $\sigma$ 161
152 17.5 h $\beta^+$ 3.0... $\gamma$ 344, 271 586... $\alpha$ ?	Tb 153 2.34 d $\alpha, \beta^+$ ... $\gamma$ 212, 110, 102 170, 83...	Tb 154 22.7 h 9.994 h 21.5 h $\beta^+$ 0.6, 1.7... $\gamma$ 879, 299 966... $\sigma$ 570	Tb 155 5.32 d $\alpha$ $\gamma$ 87, 105, 180 262...	Tb 156 5.3 h 24.4 h 5.35 d IT 88 $\beta^+$ 0.6, 1.8... $\gamma$ 123, 1274 723, 1005... e <sup>-</sup> , $\alpha$ $\sigma$ 1446	Tb 157 71 a $\alpha$ $\gamma$ (54), e <sup>-</sup>	Tb 158 10.70 s 180 a IT (110) $\beta^+$ 0.6, 1.8... $\gamma$ 879, 299 966... $\sigma$ 570	Tb 159 100 $\sigma$ 23.8	Tb 160 72.3 d $\beta^-$ 0.6, 1.7... $\gamma$ 879, 299 966... $\sigma$ 570	Tb 161 6.89 d $\beta^-$ 0.5, 0.6... $\gamma$ 26, 49, 75... e <sup>-</sup>	Tb 162 7.76 m $\beta^-$ 1.4, 2.4... $\gamma$ 260, 808 888...	Tb 163 7.76 m $\beta^-$ 0.8... $\gamma$ 351 494...
151 20 d 43	Gd 152 0.20 1.08·10 <sup>14</sup> a $\alpha$ 2.147, $\sigma$ 755 $\sigma_{n,\alpha}$ 0.007	Gd 153 240.4 d $\alpha$ $\gamma$ 97, 103, 70... $\sigma$ 22460 $\sigma_{n,\alpha}$ 0.033	Gd 154 2.18 $\sigma$ 85	Gd 155 14.80 $\sigma$ 60330 $\sigma_{n,\alpha}$ 8E-5	Gd 156 20.47 $\sigma$ 1.8	Gd 157 15.65 $\sigma$ 254000 $\sigma_{n,\alpha}$ 0.00055	Gd 158 24.84 $\sigma$ 2.22	Gd 159 18.479 h $\beta^-$ 1.0... $\gamma$ 364, 58... $\sigma$ 1.4	Gd 160 21.86 $\sigma$ 1.4	Gd 161 3.66 m $\beta^-$ 1.6, 1.7... $\gamma$ 361, 315 102... $\sigma$ 19000	Gd 162 3.66 m $\beta^-$ 1.0... $\gamma$ 442
150 36.9 a $\beta^+$ ... $\gamma$ 334 439 584...	Eu 151 47.81 $\sigma$ 4.0 + 3310 + 5920	Eu 152 96 m 9.312 h 13.517 h IT 40 $\beta^+$ 0.6, 1.8... $\gamma$ 842 963... $\sigma$ 1.8E4 $\sigma$ 1.3E4	Eu 153 52.19 $\sigma$ 312, $\sigma_{n,\alpha}$ 1E-6	Eu 154 46.0 m 8.601 a $\beta^+$ 0.6, 1.8... $\gamma$ 123, 1274 723, 1005... e <sup>-</sup> , $\alpha$ $\sigma$ 1446	Eu 155 4.753 a $\beta^-$ 0.15, 0.25... $\gamma$ 87, 105... $\sigma$ 3950	Eu 156 15.19 d $\beta^-$ 0.5, 2.4... $\gamma$ 812, 89 1231...	Eu 157 15.18 h $\beta^-$ 1.3, 1.4... $\gamma$ 64, 411, 371 55, 619..., e <sup>-</sup>	Eu 158 45.9 m $\beta^-$ 2.4, 3.4... $\gamma$ 944, 977, 898 80, 1108..., e <sup>-</sup>	Eu 159 18.1 m $\beta^-$ 2.4... $\gamma$ 68, 79, 96 146, 665...	Eu 160 30.8 s 42.6 s $\beta^-$ 2.4... $\gamma$ 173 516, 413 822... $\gamma$ 72-	Eu 161 30.8 s 42.6 s $\beta^-$ 2.4... $\gamma$ 173 516, 413 822... $\gamma$ 72-
149 3.82	Sm 150 7.37	Sm 151 94.7 a	Sm 152 26.74	Sm 153 46.284 h	Sm 154 22.74	Sm 155 22.18 m	Sm 156 9.4 h	Sm 157 8.03 m	Sm 158 5.30 m	Sm 159 11.37 s	Sm 160 11.37 s

Might create long-lived waste

Might reduce production yield

# Stable isotope enrichment

- High radionuclidic purity and specific activity required  
→ (Highly) enriched isotopes needed
- Enrichment techniques
  - **Distillation** – only works effectively when large relative mass differences between different isotopes of an element → light isotopes
  - **Gaseous centrifugation** – only works when gaseous compound of the element exists. Most cost-efficient for enrichment of elements too heavy for distillation
  - **Electromagnetic isotope separator (EMIS)** – magnetic and electronic forces separate charged isotopic species. More costly to operate and smaller production quantities



# Stable isotope enrichment

H																	He
Li	Be											B	C	N	O	F	Ne
Na	Mg											Al	Si	P	S	Cl	Ar
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
Cs	Ba	*	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
Fr	Ra	**															

\* Lanthanides

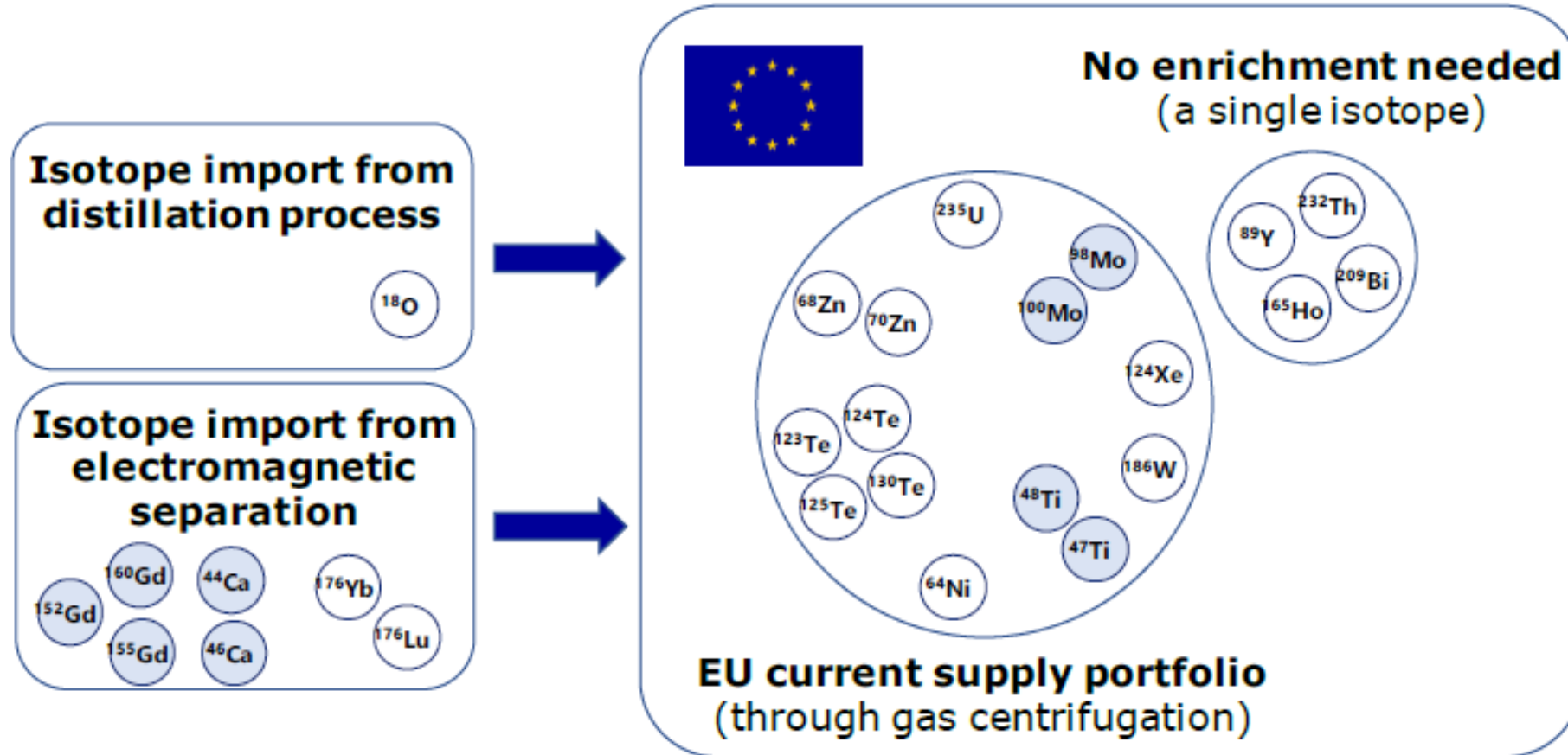
La	Ce	Pr	Nd	Pm	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu
Ac	Th	Pa	U	Np	Pu	Am	Cm	Bk	Cf	Es	Fm	Md	No	Lr

\*\* Actinides

Ne	Enrichment by distillation, chemical or photochemical method
Ar	Enrichment by centrifugation

Cu	Enrichment by electromagnetic method
Y	No enrichment possible, only a single isotope in natural product

# Stable isotope enrichment





# Target

Target manufacturing  
and irradiation

Radiochemical  
processing

Quality control

Target recovery and  
recycling

Waste management

## Target material scarcity

Scarcity of highly enriched target material

- High enrichment factor and high chemical purity needed
- Very high dependency on Russian calutrons (WWII era technology)
  - Can separate almost every stable isotope, but costly to operate and relatively small quantities only
  - Market dominated by Russia
  - Situation is slowly changing – but new initiatives are expensive and time-consuming
  - Most initiatives focused on  $^{176}\text{Yb}$  supply for  $^{177}\text{Lu}$  production

# Neutron activation

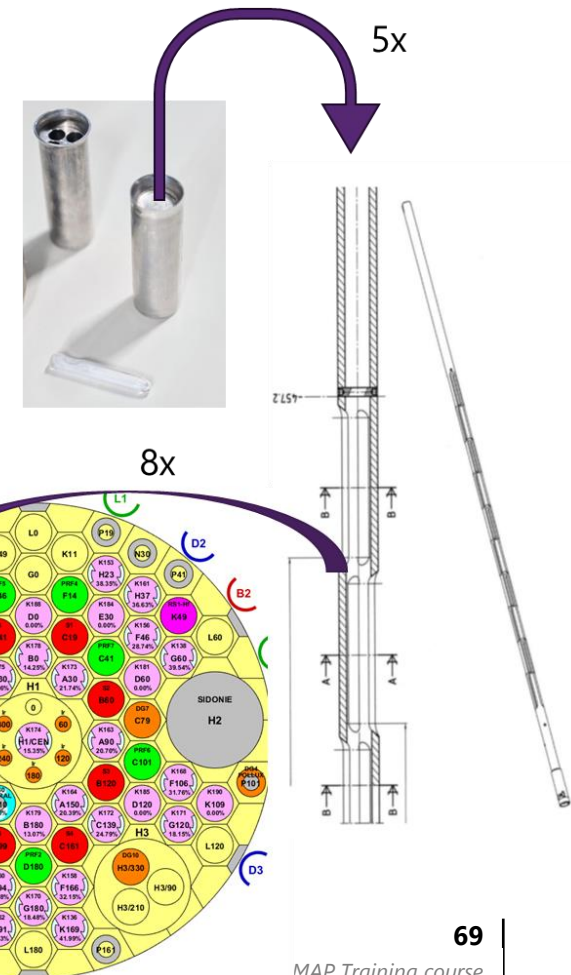
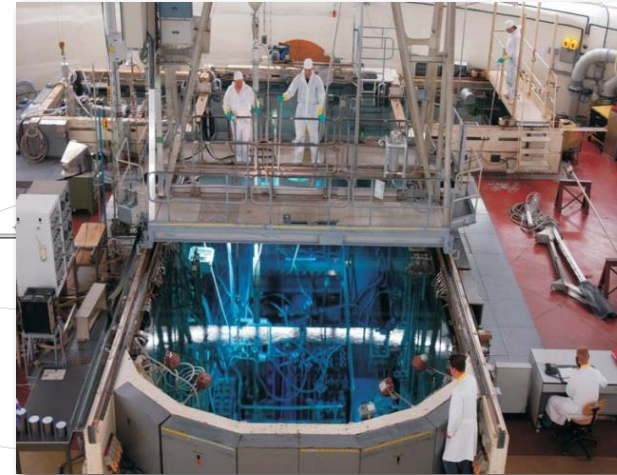
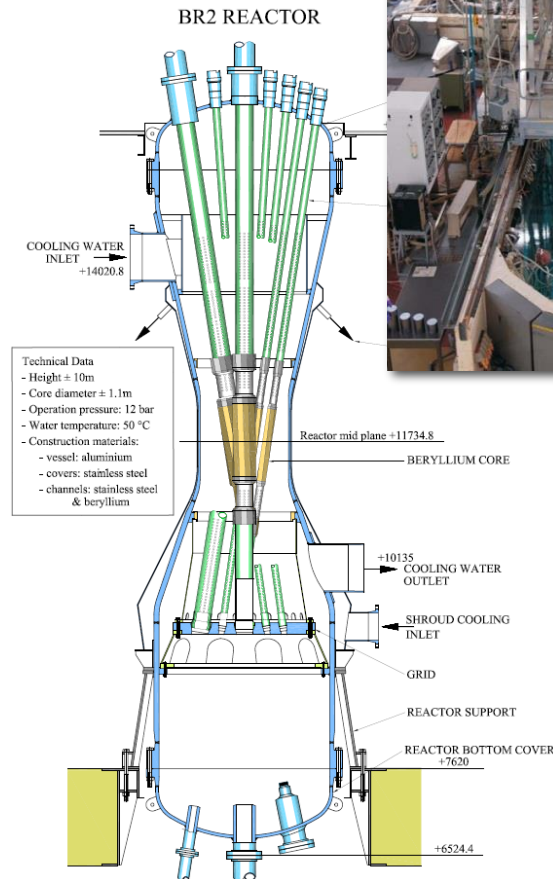
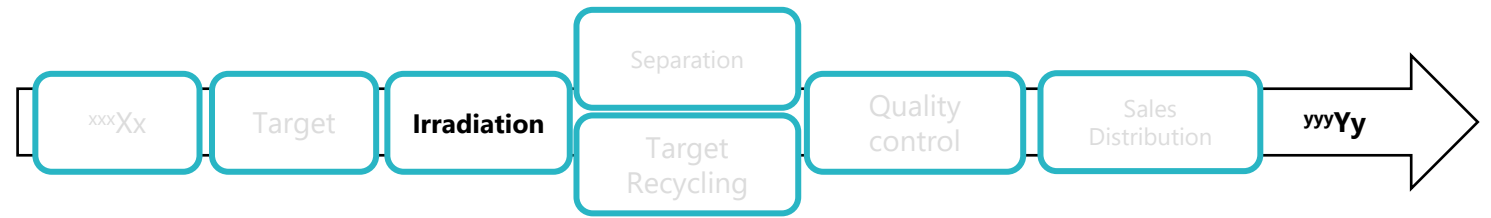
Target manufacturing and irradiation

Radiochemical processing

Quality control

Target recovery and recycling

Waste management





# Neutron activation

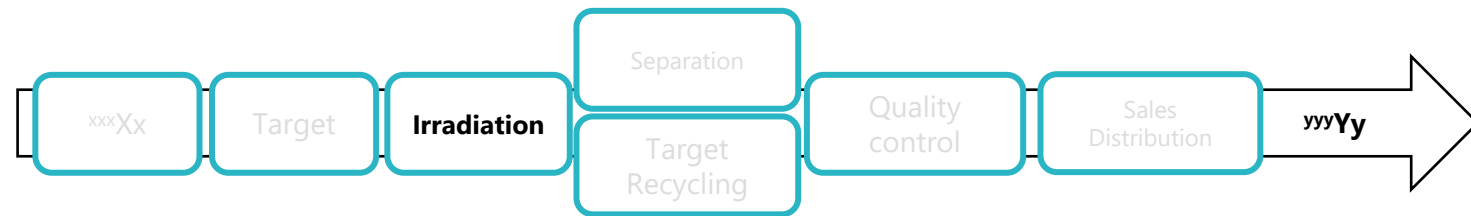
Target manufacturing and irradiation

Radiochemical processing

Quality control

Target recovery and recycling

Waste management



Transfer of irradiated targets to hotcell for decanning

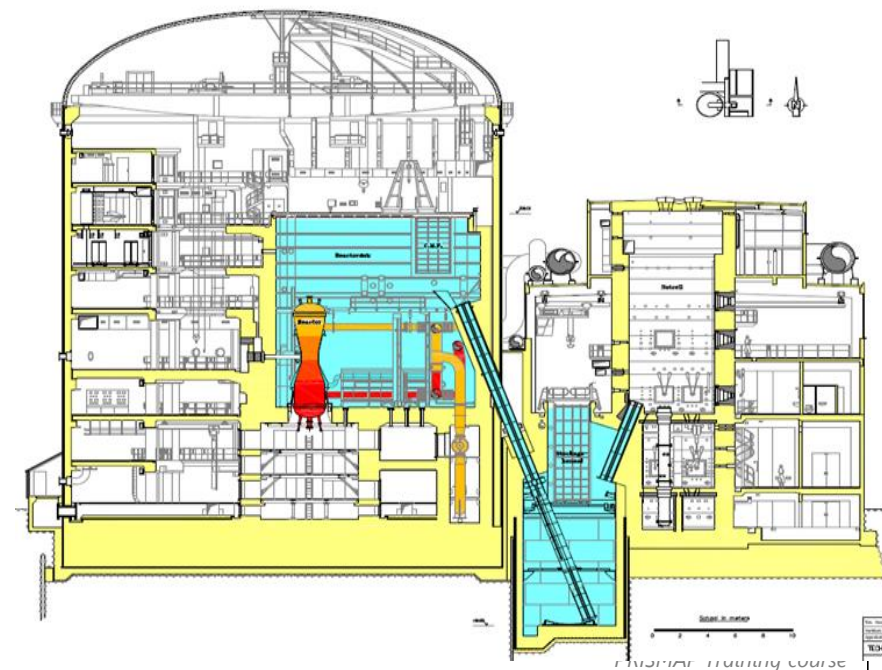
- Cooling of irradiated targets → *decay of short-lived radio-contaminants*
- Opening of aluminium irradiation can
- Preparation for shipment in dedicated transport containers



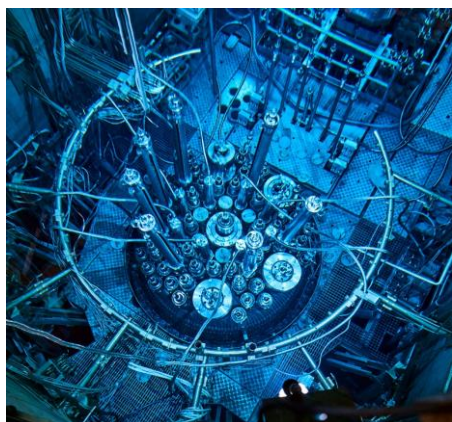
Type A ( $\leq 700$  GBq  $^{177}\text{Lu}$ )



Type B ( $> 700$  GBq  $^{177}\text{Lu}$ )



# Transport of activated target material



**Reactor**



**Radiochemical  
processing facility**



# RADIO CHEMISTRY

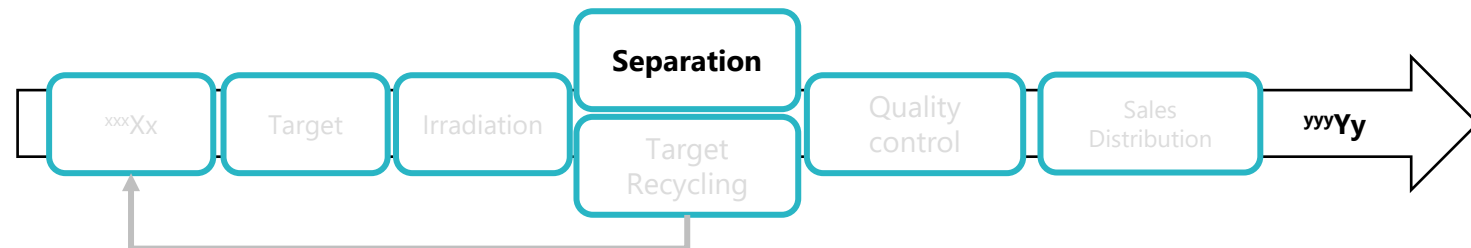
Target manufacturing  
and irradiation

Radiochemical  
processing

Target recovery and  
recycling

Quality control

Waste management



- Isolate radionuclide from target matrix
- Develop efficient separation methods, guaranteeing
  - High quality end-product
  - High target recovery and regeneration
  - Appropriate waste management
- Easy scale-up and cost-efficient
  - MBq scale → GBq scale
  - GBq scale → TBq scale
  - Simple, robust and fast
  - Automated and remote-controlled
  - Insensitive to target contaminants
  - GMP compliant



Lu:Yb ratio 1:10<sup>4</sup>-10<sup>6</sup>



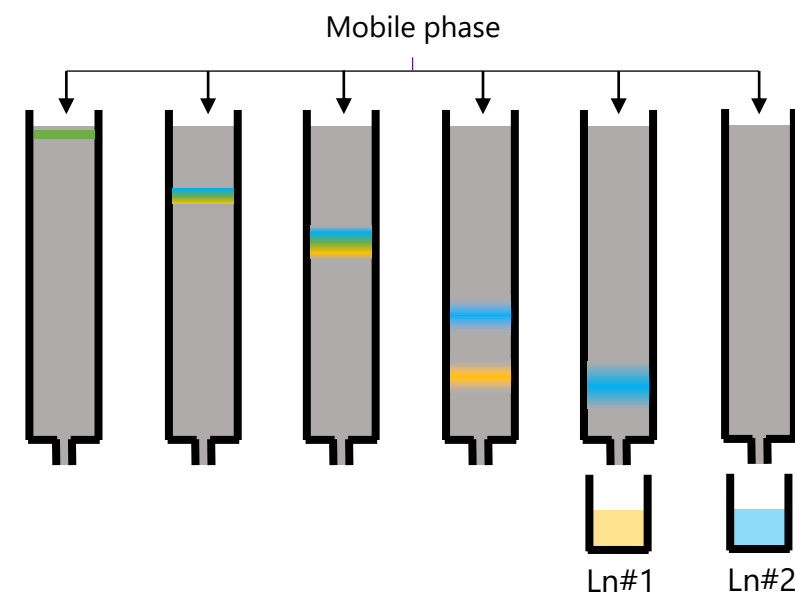
# Lanthanides – Separation strategies

## Small difference in affinity for coordinating ligands

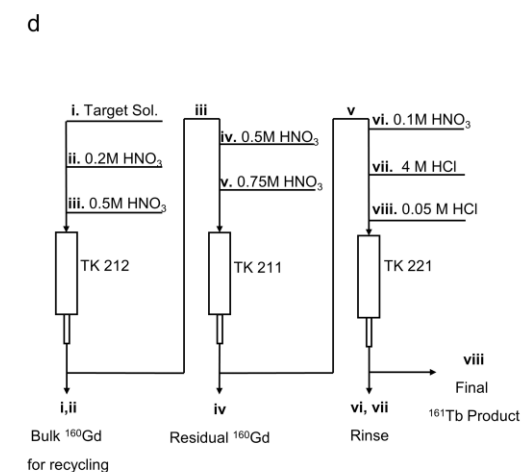
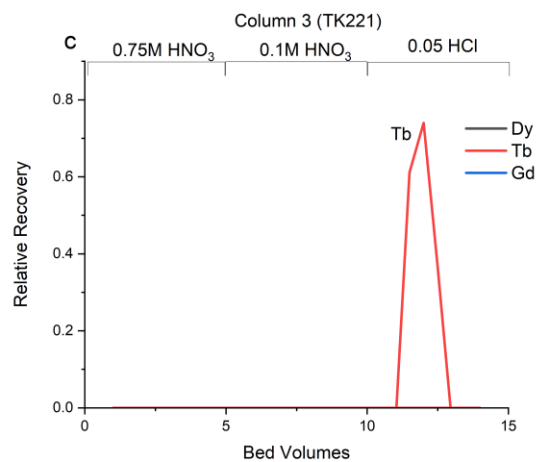
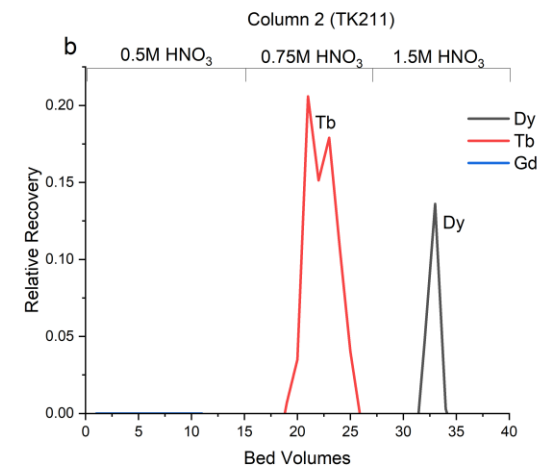
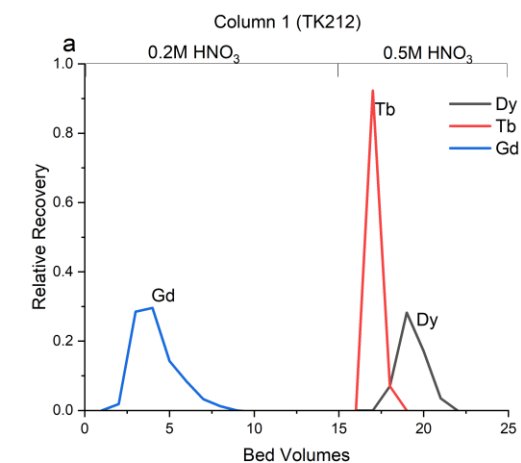
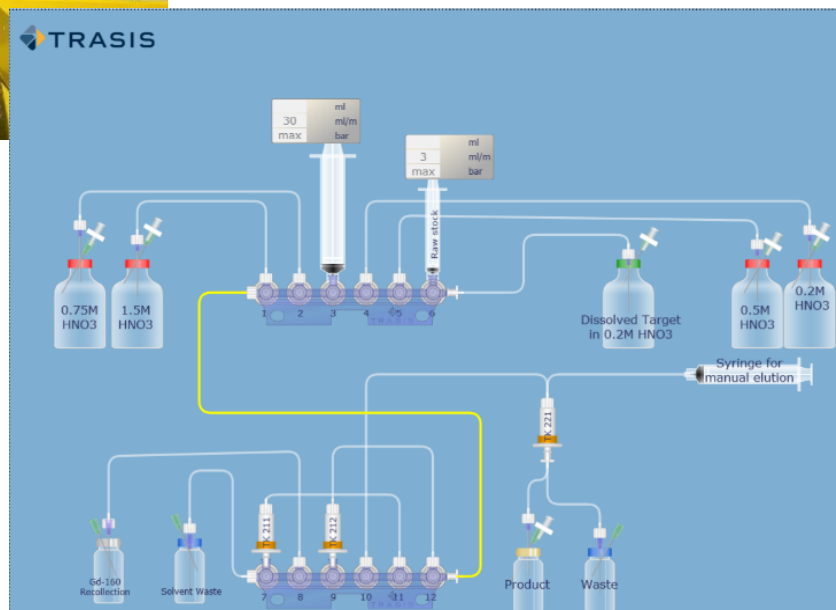
- Extraction chromatography
  - Extractant physically impregnated onto solid support
  - Heavier lanthanide binds stronger to extractant
  - Lighter lanthanide elutes first
- Strong cation exchange
  - Functional groups resin (usually  $\text{SO}_3^-$ )
  - Chelating ligand in mobile phase
  - Heavier lanthanide binds stronger to chelating ligand
  - Heavier lanthanide elutes first

⇒ Obtain high-purity fractions

⇒ Separate micro amounts for macro amounts



# Extraction chromatography method



# Strong cation exchange method

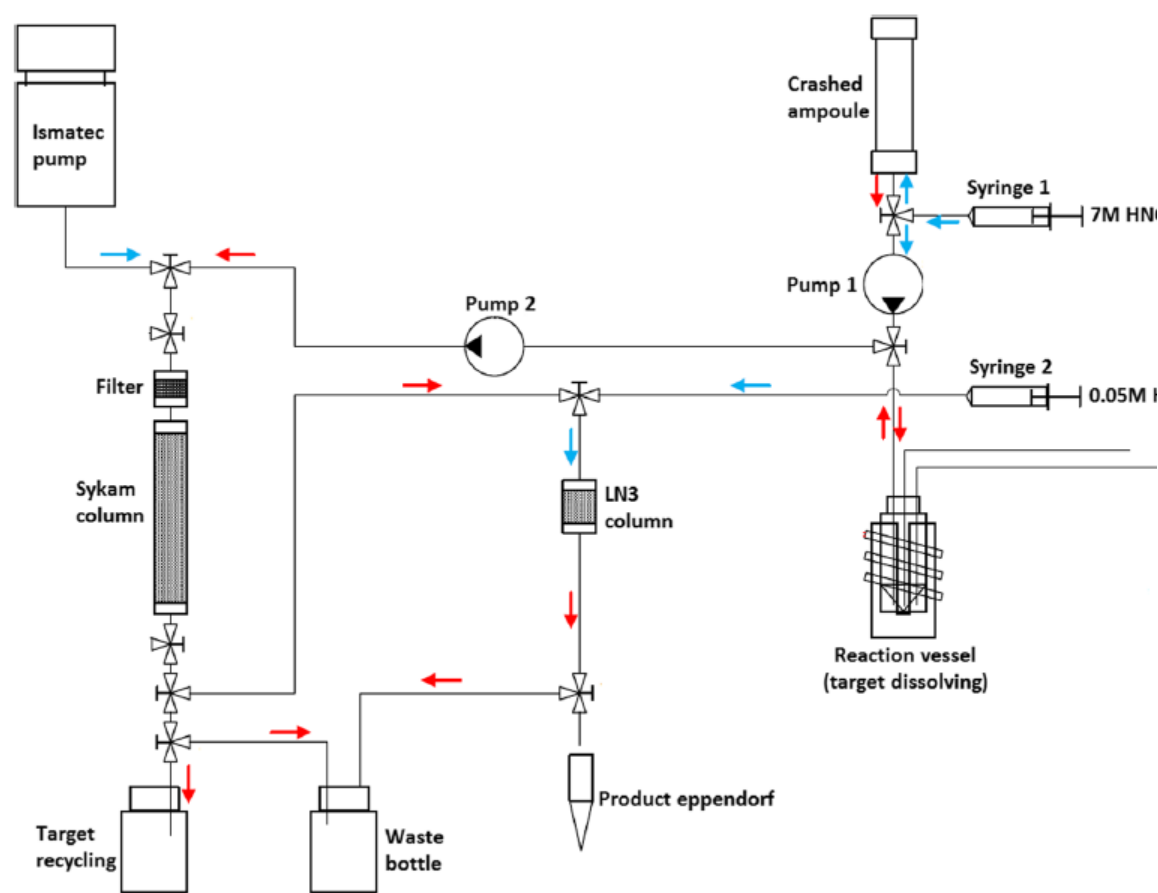


Fig. 2 Schematic diagram of the  $^{161}\text{Tb}$  chemical separation system

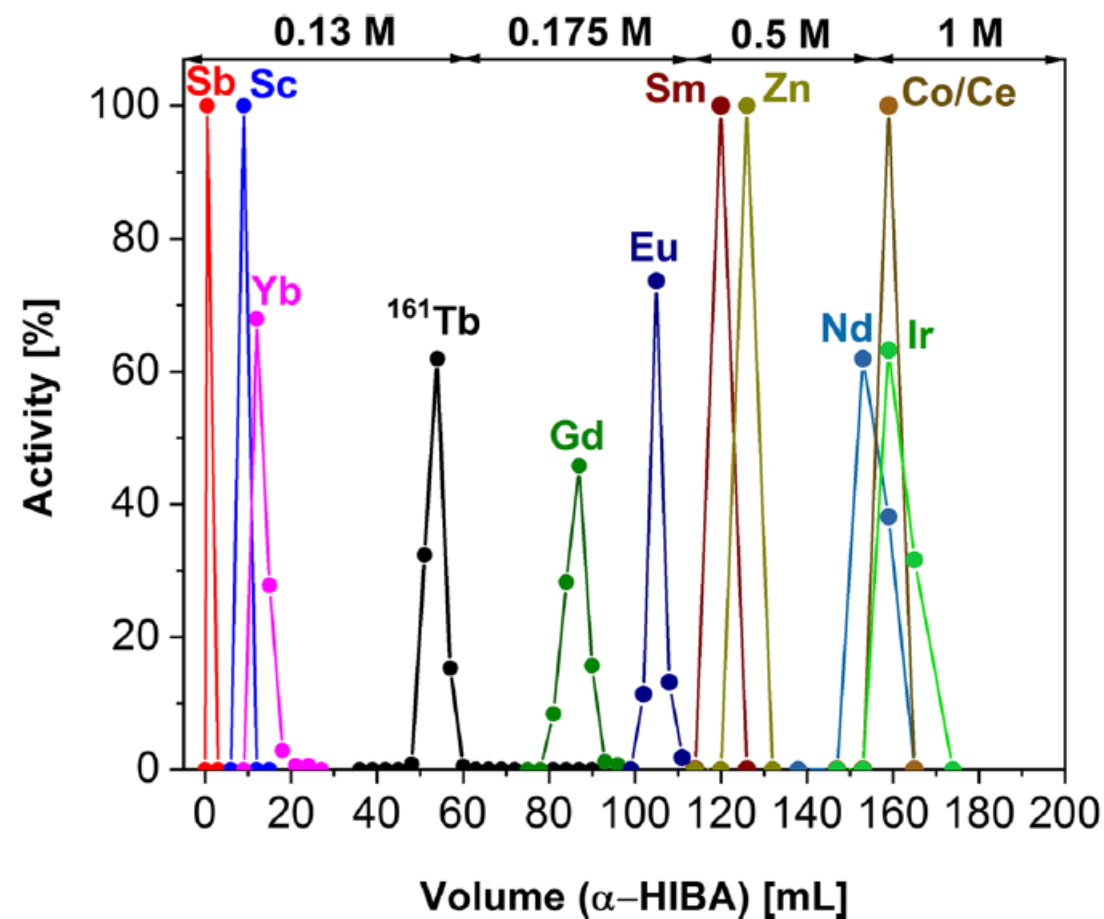


Fig. 1 Elution profile of  $^{161}\text{Tb}$  separation from the irradiated target material and side products (10 mm x 170 mm Sykam resin column, 8 mg  $^{160}\text{Gd}_2\text{O}_3$ , 0.6 mL/min eluent flow rate)

# RADIO CHEMISTRY

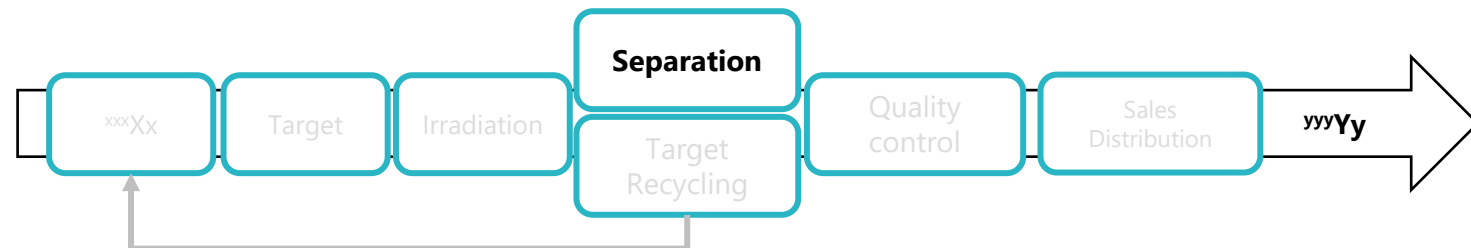
Target manufacturing  
and irradiation

Radiochemical  
processing

Target recovery and  
recycling

Quality control

Waste management



Production environment – typically hot cells in a clean room facility

- Lead shielded hot cells
- Processes (fully) automated
- Hot cells equipped with telemanipulators for remote handling





# RADIO CHEMISTRY

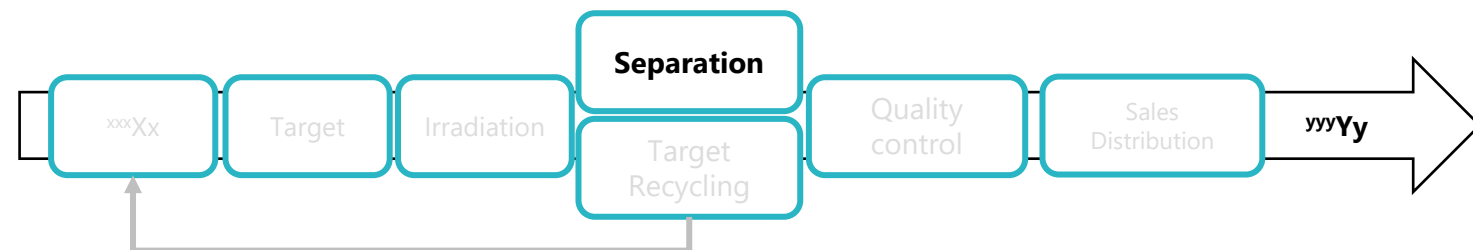
Target manufacturing  
and irradiation

Radiochemical  
processing

Target recovery and  
recycling

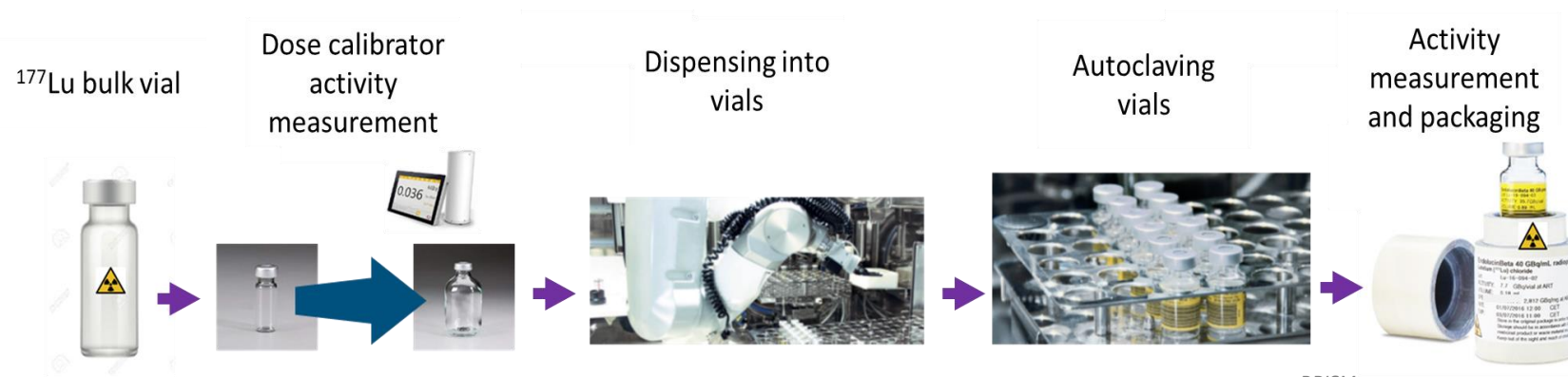
Quality control

Waste management



Production environment – typically hot cells in a clean room facility

- Lead shielded hot cells
- Processes (fully) automated
- Hot cells equipped with telemanipulators for remote handling
- Dispensing and sterilization
- Packaging





# Quality control

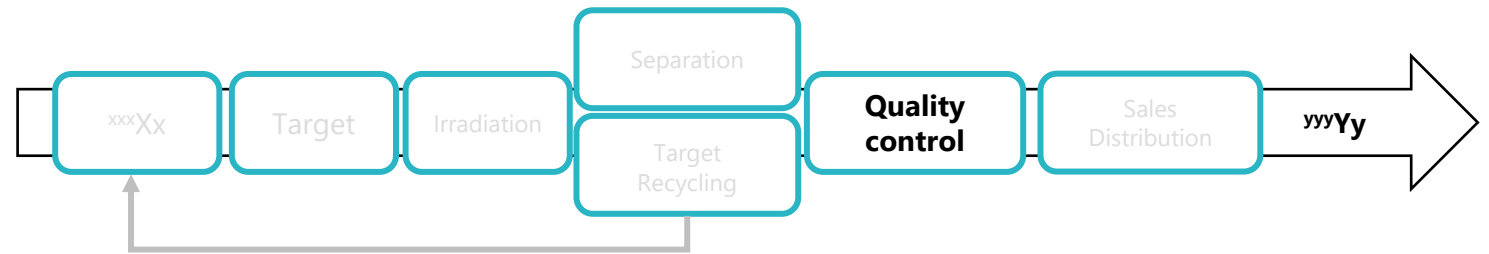
Target manufacturing and irradiation

Radiochemical processing

Quality control

Target recovery and recycling

Waste management



- High quality product – Tested according to Eur. Phar. guidelines
- Needed to guarantee product quality for medical use
  - Radionuclidic purity (*gamma spectrometry*)
  - Chemical purity (*ICP-MS/ICP-OES*)
  - Radiochemical purity (*radio-TLC*)
  - Activity concentration (*dose calibrator*)
  - Specific activity (*dose calibrator + ICP-MS/ICP-OES*)
  - Radiolabeling (apparent molar activity) (*radio-TLC*)
  - Biocompatible (endotoxin + sterility)
- Certificate of analysis

# Quality control

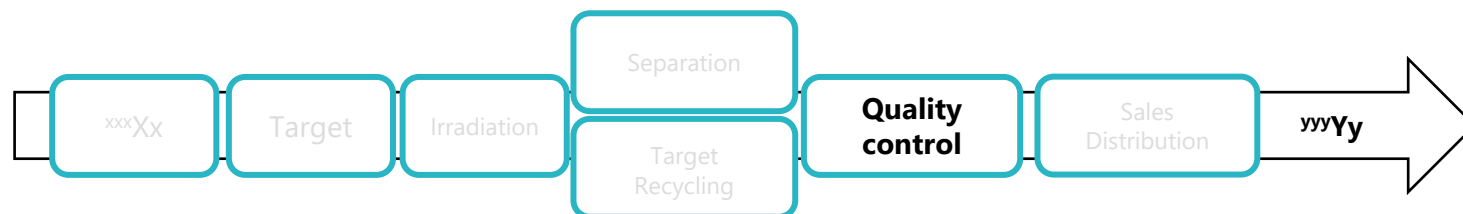
Target manufacturing and irradiation

Radiochemical processing

Quality control

Target recovery and recycling

Waste management



## Certificate of Analysis

EndolucinBeta 40 GBq/ml Radiopharmaceutical precursor solution

Lot No.:	Lu-22-348-01	Time of Manufacturing [CET]:	13.06.2022 11:00
Serial No.:	11103081-0-0		
Customer:	SCK-CEN		
Activity [GBq]:	9.3	ART [CET]:	20.06.2022 12:00
Volume [µl]:	238	Expiry Date [CET]:	22.06.2022 11:00
Chemical Form:	Lu (3+) in aqueous 0.04 M HCl solution		
Packaging:	2 ml type I glass vial, closed with fluorotec coated bromobutyl septum and center hole crimp cap		

Test	Specification	Unit	Result
Activity per Vial	<sup>1</sup> 90 - 110 of the activity stated on the label	%	complies
Radioactivity Concentration (Dose Calibrator)	<sup>1</sup> 36 - 44	GBq/ml	39
Appearance	Clear and colorless solution	n.a.	complies
Identity Lu-177 (Gamma spectrometry)	113 keV gamma line existing 208 keV gamma line existing	n.a.	complies
Identity Chloride (Ph. Eur.)	White precipitate visible	n.a.	complies
pH value (pH indicator strips)	1 - 2	n.a.	complies
Specific Activity (ICP-MS)	<sup>2</sup> ≥ 3000	GBq/mg	3020
Chemical Purity (ICP-MS) corrected to Lu-177 activity at EOS	Fe ≤ 0.25 Cu ≤ 0.5 Zn ≤ 0.5 Pb ≤ 0.5 Yb-176 ≤ 0.14 Sum of impurities ≤ 0.5	µg/GBq µg/GBq µg/GBq µg/GBq µg/GBq µg/GBq	<0.01 <0.1 <0.1 <0.1 <0.01 <0.1
Radionuclidic Purity (Gamma spectrometry) corrected to Lu-177 activity at EOS	<sup>3</sup> Yb-175 ≤ 0.01 Sum of other impurities ≤ 0.01	% %	<0.01 <0.01
Radiochemical Purity (TLC)	≥ 99.0 as 177LuCl3	%	100.0
Radiolabeling Yield (TLC) based on radiolabeling with Lu-177 of DOTA-derivate, molar ratio 1:4	≥ 99.0	%	99.9
Bacterial Endotoxins (Ph. Eur.)	≤ 20	EU/ml	<2
Sterility (Ph. Eur.)	Sterile	n.a.	Sample taken

<sup>1</sup> Result taken from In-Process Control, value decay-corrected to ART  
<sup>2</sup> Result taken from Release / Retest of API, value decay-corrected to ART  
<sup>3</sup> Result taken from Release / Retest of API, value decay-corrected to EOS

ART: Activity reference time  
 EOS: End of shelf life  
 \*\* OOS Result

This batch complies with the specification.



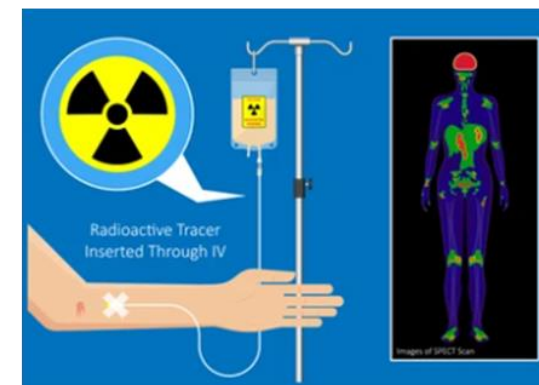
# Transport of purified radionuclide



**Radiochemical  
processing facility**



**Radiopharmaceutical  
company**



**Hospital**



# Target recycling

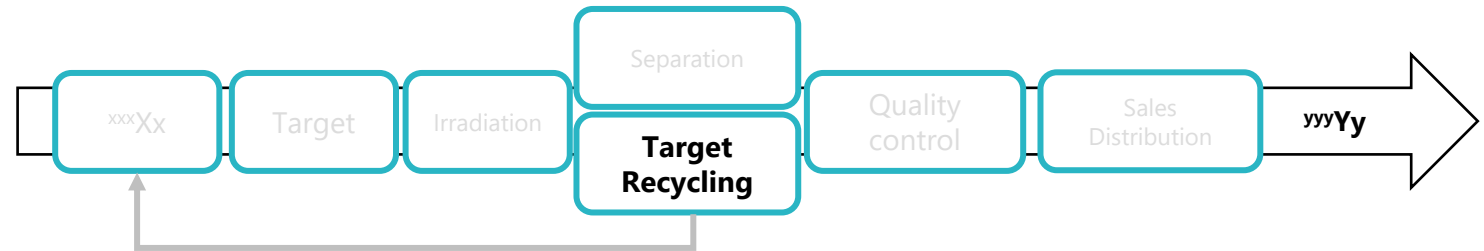
Target manufacturing and irradiation

Radio-chemical processing

Quality control

Target recovery and recycling

Waste management



- Target material is scarce and highly valuable
- Needs to be recovered from separation process matrix
  - Conversion to the oxide (or other suitable compound)
- Needs to be suitable for re-irradiation, i.e. safe handling by reactor operators (acceptance criteria set by reactor management)
  - Removal of long-lived radio-contaminants
    - Decay strategy
    - Reprocessing strategy
- Proper characterization and QC

# Waste management

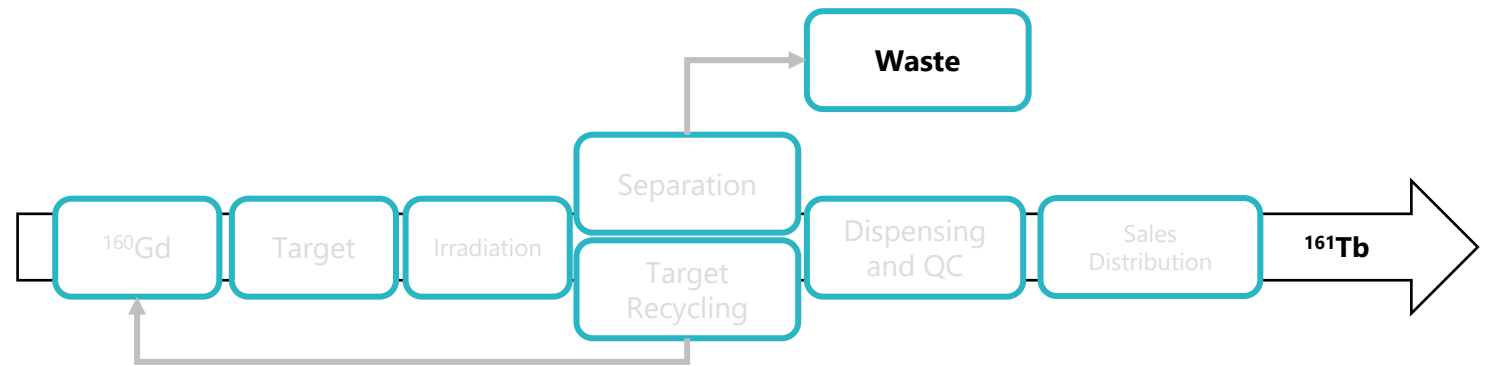
Target manufacturing and irradiation

Radio-chemical processing

Quality control

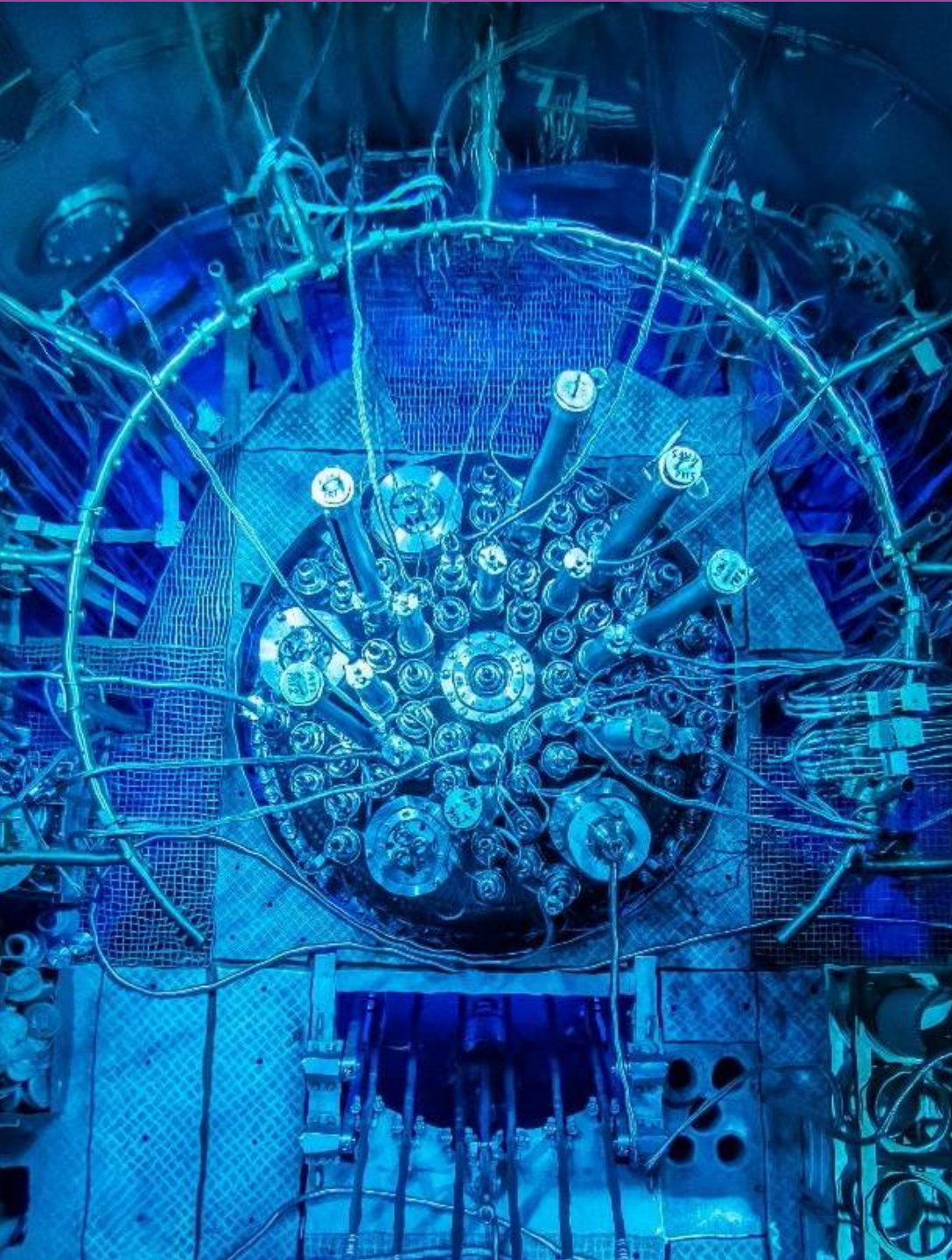
Target recovery and recycling

Waste management



- Identification of long-lived radio-contaminants in each fraction
  - Depends on purity of target material
- Appropriate waste collection and treatment strategies
  - Liquid waste
  - Solid waste
- Appropriate selection of materials used for irradiation (e.g. quartz quality)
  - To be considered during design of the radiochemical process and selection of appropriate target material!





# Conclusions

- High thermal neutron fluxes are required for efficient production of radionuclides
- Two major production pathways
  - $^{235}\text{U}(n,f) \rightarrow$  Major production route for  $^{99}\text{Mo}/^{99\text{m}}\text{Tc}$
  - Neutron activation  $\rightarrow$  Predominantly therapeutic radionuclides
- Supply chain can be complex, and is a race against time
- Simple, robust and scalable radiochemistry steps
- High target quality is key
- Both research reactors and accelerators/cyclotrons are needed for nuclear medicine

**Nuclear research reactors are  
powerfull thermal neutron sources**

**Crucial for manufacturing of  
medical radionuclides**





 [WWW.PRISMAP.EU](http://WWW.PRISMAP.EU)

 [@MEDRADIONUCLIDE](https://twitter.com/MEDRADIONUCLIDE)

 [PRISMAP PROJECT](#)



This project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101008571 (PRISMAP)

## Copyright © SCK CEN

All property rights and copyright are reserved.

This presentation contains data, information and formats for dedicated use only and may not be communicated, copied, reproduced, distributed or cited without the explicit written permission of SCK CEN.

If this explicit written permission has been obtained, please reference the author, followed by 'by courtesy of SCK CEN'.

Any infringement to this rule is illegal and entitles to claim damages from the infringer, without prejudice to any other right in case of granting a patent or registration in the field of intellectual property.

### **SCK CEN**

Studiecentrum voor Kernenergie  
Centre d'Etude de l'Energie Nucléaire  
Belgian Nuclear Research Centre

Stichting van Openbaar Nut  
Fondation d'Utilité Publique  
Foundation of Public Utility

Registered Office: Avenue Herrmann-Debrouxlaan 40 - 1160 BRUSSELS - Belgium

Research Centres: Boeretang 200 - 2400 MOL - Belgium

Chemin du Cyclotron 6 -1348 OTTIGNIES-LOUVAIN-LA-NEUVE - Belgium